

UNCLAS



**GEMINI PROPULSION
TECHNICAL REVIEW MEETING**

9-12 FEBRUARY 1965



**BELL
AEROSYSTEMS
COMPANY**

DIVISION OF BELL AEROSPACE CORPORATION

A
textron
COMPANY

GEMINI PROPULSION SYSTEM
MULTI-START ENGINE
BAC MODEL 8247
USAF MODEL XLR 81-BA-13

SYSTEM REQUIREMENTS

	8096	8247
NUMBER OF STARTS	ENGINE (MISSION)	2
	ENGINE (NOMINAL)	15
	THRUST CHAMBER	25
	NOZZLE EXTENSION	2
MINIMUM TOTAL IMPULSE	—	17,500 lb SEC
PROPELLANT UTILIZATION	START lb.	12 OX
	SHUTDOWN (OX) lb.	35
START SYSTEM LOAD & PAD HOLD	DRY	WET
ELECTRICAL CHARACTERISTIC	—	EMI
RELIABILITY DEMONSTRATION	.997	NONE
	@ 90%	REQ'D
	CONFIDENCE	
	LEVEL	

MODEL 8247 ENGINE

DESCRIPTION AND OPERATION

SYSTEM REQUIREMENTS

ENGINE TESTING

DEMONSTRATION

ENGINE XRM1 70 FIRINGS @ 110,000 FT ALT.

ENGINE XRM2 80 FIRINGS

ENGINE XRM3 61 FIRINGS

QUALIFICATION - PFRT

ENGINE S/N 801 36 FIRINGS

WEIGHT HIGH TEMPERATURE

DRAINAGE HUMIDITY

VIBRATION LOW TEMPERATURE

SHOCK MALFUNCTION

FIXED THRUST CALIB. DISASSEMBLY & INSPECTION

PFRT PROBLEM AREA

DUAL CHECK VALVE

GAS GENERATOR SOLENOID VALVES

START TANKS

TURBINE PUMP DEVELOPMENT TESTING
MULTIPLE RESTART

MODEL 8247

I EXPLORATORY TESTS

A START TANK SYSTEM - 59 RUNS - 106 STARTS - 1210 SEC.

1. START TRANSIENTS
2. SHUTDOWN TRANSIENTS
3. OXIDIZER CRACKING PRESSURE EFFECT
 - a) PROPELLANT PRE-FLOW
 - b) PROPELLANT POST FLOW
4. START TANK BLOWDOWN AND RECHARGE
 - a) AT HIGH TEMPERATURE
 - b) AT LOW TEMPERATURE
5. RESTART AFTER VERY SHORT DURATION RUN
 - a) AT AMBIENT TEMPERATURE
 - b) AT +10°F TEMPERATURE

B PUMP SUCTION PRESSURE START SYSTEM

39 RUNS - 39 STARTS - 1471 SECONDS

- I. ENVIRONMENTAL LIMITS ON START TRANSIENTS
 - a) OXIDIZER PUMP SUCTION PRESSURE
 - b) FUEL PUMP SUCTION PRESSURE
 - c) OXIDIZER PROPELLANT TEMPERATURE
 - d) FUEL PROPELLANT TEMPERATURE
 - e) HARDWARE TEMPERATURE
 - f) TURBINE STATIC FRICTIONAL TORQUE

C CONCLUSION

START TANK SYSTEM MET ALL ASPECTS OF THE MULTIPLE RESTART REQUIREMENTS.

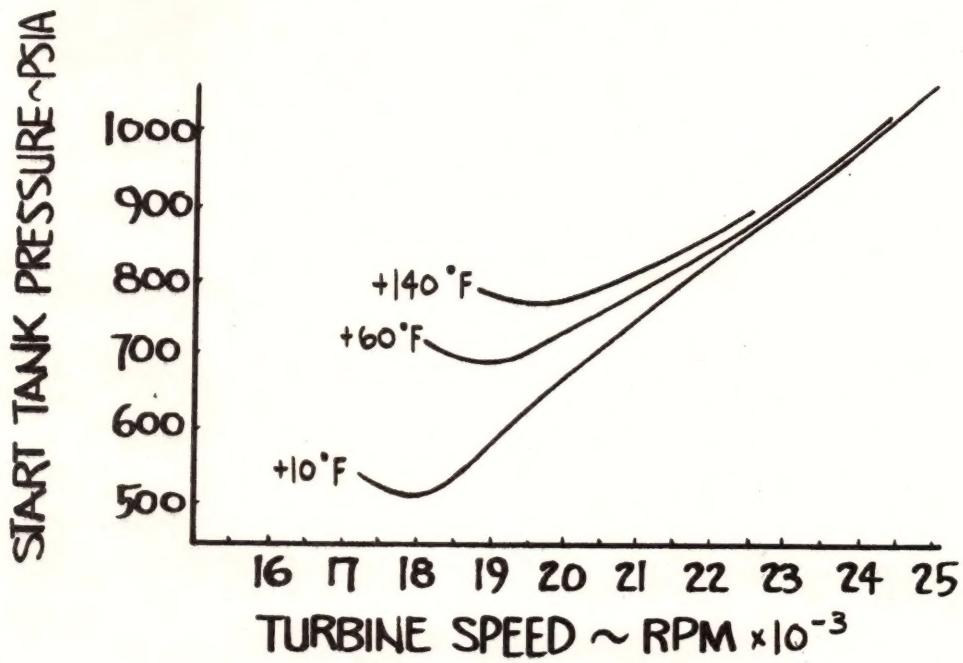
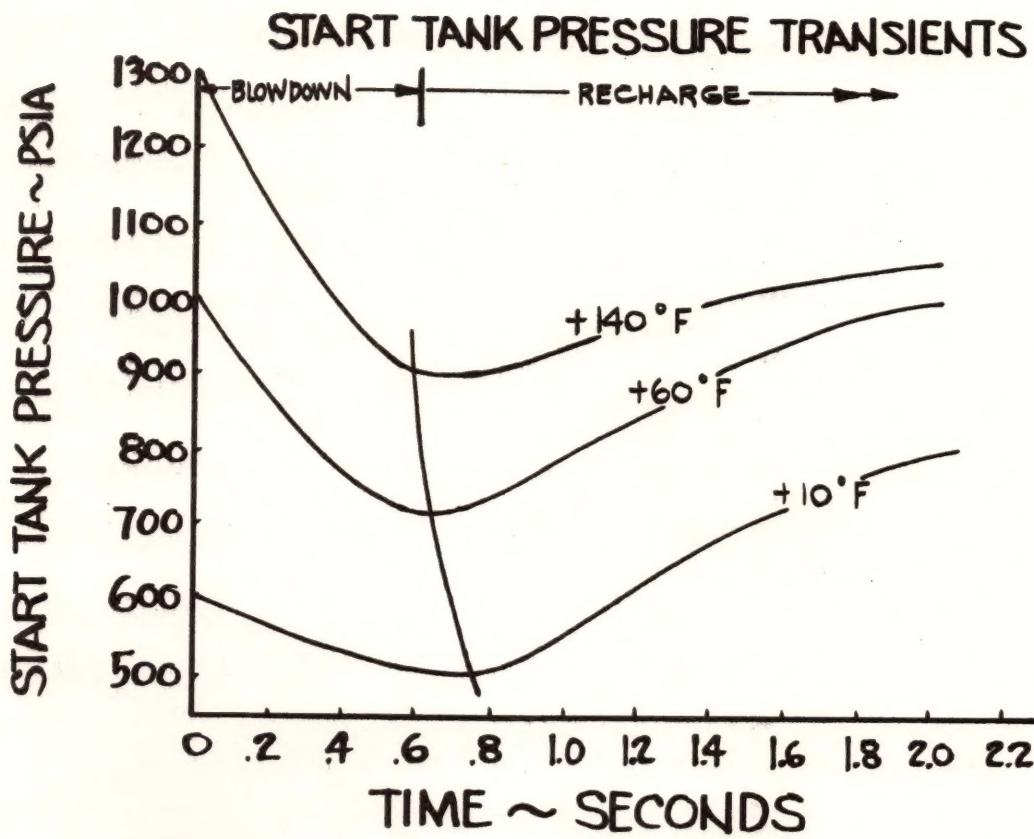
II DEVELOPMENTAL TESTS

A BOILER PLATE TYPE HARDWARE, 25 RUNS- 49 STARTS- 1876 SEC.

1. START AND SHUTDOWN TRANSIENTS
2. START TANK BLOWDOWN AND RECHARGE
3. MALFUNCTION TESTS
4. GAS ENTRAPMENT IN START TANK SYSTEM

B PROTO TYPE HARDWARE 200 RUNS 453 STARTS 15,422 SEC.

1. FUEL VALVE OPENING EFFECT
2. START AND SHUTDOWN TRANSIENTS
 - a "BIT IMPULSE" DURATION
 - b TEMPERATURE EFFECT
 - c START TANK PROPELLANT LOADING
3. GAS GENERATOR VALVE EVALUATION
4. MALFUNCTION TESTS



MODEL 8247 START TANK SIZING

A OBJECTIVES

1. TO DETERMINE FUEL AND OXIDIZER START TANK SIZES
2. TO ESTABLISH LOAD CONDITIONS AT 60°F TO SATISFY
OPERATION FOR:
 - a TEMPERATURE RANGE OF +10°F TO +140°F
 - b MINIMUM ENGINE IMPULSE OF 16,000 LB-SEC
AND STEADY STATE RUN IMPULSE

B VARIANCES CONSIDERED

1. FLIGHT SPEED	± 3 %
2. LOADING	± 2 %
3. MAXIMUM PROPELLANT LEAKAGE	1 IN ³

C OPERATING SEQUENCE

1. LOAD NOMINAL AT 60°F
2. RUN TO STEADY STATE AT 50°F
3. RUN TO MINIMUM "BIT-IMPULSE" AT +140°F
4. RUN TO STEADY STATE AT -10°F MAXIMUM SPEED
5. CONDITION SYSTEM TO +140°F

THRUST CHAMBER TESTING

THRUST CHAMBER PFRT (8096)

OBJECTIVES

1. DEFINE THRUST VARIATION WITH CHAMBER PRESSURE($P_c \pm 5\%$ /RATED) WITHOUT NOZZLE EXTENSION
2. DEMONSTRATE FIRING OF NOZZLE EXTENSION IN ASPIRATOR DUCT AFTER TEMPERATURE CYCLING

TESTS CONDUCTED

<u>CONDITION</u>	<u>% RATED P_c</u>	<u>NO TESTS</u>
BASIC CHAMBER	100	2
BASIC CHAMBER	95	2
BASIC CHAMBER	105	2
BASIC CHAMBER PLUS NOZZLE EXTENSION	100	2

RESULTS

1. THRUST vs P_c ESTABLISH = $27.88 \text{#F/PSI } P_c$
2. NO DETRIMENTAL EFFECTS OF TEMPERATURE CYCLING ON A NOZZLE EXTENSION TESTED IN AN ASPIRATOR DUCT.

PRESSURE SWITCH REMOVAL PROGRAM

OBJECTIVE

DEMONSTRATE FUEL LEAD

ANALYSIS

FUEL LEAD OF .16 TO .205 SECONDS

TEST PROGRAM

Nº TESTS 58

Nº CHAMBERS 2

DEMONSTRATED

	FEED PRESSURE	FUEL LEAD RANGE	TEMPERATURE	Nº TESTS
1ST BURN	80-130% RATED	.04 to 1.0	AMB-140°F	31
2ND BURN	RATED (400PSI)	.10 to .97	-2°F-150°F	14

DEFINED ACCUMULATION EFFECTS OF FUEL LEAD

NONE

Pc OVER SHOOT ON START

RANGE %

OX LEAD 34 TO 49

1ST BURN FUEL 02 TO 24

2ND BURN FUEL 16 TO 38

ALTITUDE TESTING

AEDC

MODEL 8247 START TANKS

A - COMPONENT REVIEW

I - THE QUALIFICATION OF THE START TANKS WAS PERFORMED DURING THE FLIGHT VERIFICATION TEST PROGRAM.

THE FVT TESTS WERE:

I STRUCTURAL INTEGRITY (2 SETS OF SHELLS)

SET #1 - AFTER 30 DAY SALT WATER EXPOSURE
AT MAXIMUM STRESS.

SET #2 - IN THE "AS RECEIVED" CONDITION.

II DESIGN OBJECTIVES & DYNAMICS (2 SETS OF ASSEMBLIES)

SET #1 a) MALFUNCTION PRESSURES

b) DUTY CYCLES

c) DYNAMICS (MODEL SPEC LEVELS)

d) BELLOW'S YIELD

e) STRUCTURAL INTEGRITY

f) METALLURGICAL EVALUATION

SET #2

a) SIMULATED SHIPPING PRESSURES TEST

b) DUTY CYCLES (10)

c) BELLOW'S LIFE CYCLE

d) STRUCTURAL INTEGRITY

e) METALLURGICAL EVALUATION

III COMPATABILITY

a) OXIDIZER START TANK SYSTEM IN 38 DAY PAD STORAGE TEST

b) OXIDIZER BELLOW'S FROM ENGINE #802

IV DEVELOPMENT PROBLEMS & CORRECTIVE ACTION

D.P.- BELLows STICKING OR HANGING UP

C.A. { a) IMPROVED SURFACE FINISHES
b) CONFIGURATION CHANGE TO FLAT HEAD
c) LUBRICATION
d) CLOSURE WELD FIXTURING IMPROVEMENT
e) FILTER IN GAS PORT

D.P.- SHELL CRACKS & LEAKAGE

C.A. { a) CLOSED DIE FORGING WITH ORIENTED GRAIN
b) TIGHTER MATERIAL CONTROL, CHEMISTRY
& HEAT TREATMENT

D.P. - LEAKAGE IN FUEL BELLows & END MEMBERS

a) CLOSED DIE FORGING WITH ORIENTED GRAIN
b) TIGHTER MATERIAL CONTROL , CHEMISTRY
& HEAT TREATMENT.
c) INCREASED THE LEAKAGE PATH WITH
THICKER BELLows ATTACHMENT AREAS.

2 -THE FOLLOWING CHANGES HAVE BEEN MADE SINCE QUALIF.

-SOME RELAXATION OF METALLURGICAL REQUIREMENTS,
I.E., 2% TO 3% DELTA FERRITE & 4 TO 3 GRAIN SIZE.

3- THE FOLLOWING CONFIGURATIONS ARE BEING DELIVERED TO LMSC.

8247-471201-1 OXDR TANK & 8247-471202-1 FUEL TANK

4-NOT APPLICABLE (SYSTEMS GROUP)

5-PROBLEM AREAS , PAST AND PRESENT

a) SCRATCHES & CONTAMINANTS CAUSING BELLows STICKING
b) STRESS CORROSION & INTERGRANULAR CORROSION CRACKING
c) DISTORTION & MISALIGNMENT OF SHELLS AT CLOSURE WELDING

MODEL 8247 START TANKS

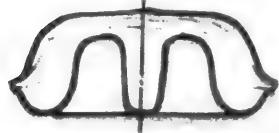
FABRICATION CONTROL: AM 355

I PARENT BILLET.

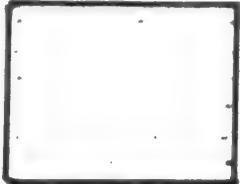
- A. BILLET STOCK IS PRODUCED BY THE COMSUMABLE ELECTRODE REMELT TECHNIQUE UNDER INERT GAS OR VACUUM.
- B. METALLOGRAPHIC SAMPLES ARE CUT FROM EDGE AND CENTER, AND THE MICROSTRUCTURE CHECKED TO ASSURE THAT IT IS FREE OF MASSIVE CARBIDES WHICH WILL NOT GO INTO SOLUTION WITH HEAT TREATMENT.
- C. A ONE INCH THICK BLANK IS HEAT TREATED AS IN ITEM ID, PRIOR TO FORGING, AND CHECKED FOR CONFORMANCE TO THE MECHANICAL PROPERTIES REQUIRED.
- D. HEAT TREAT TO 1900°F FOR 3 TO 3½ HOURS. RAPID QUENCH & SUB ZERO COOL AT -100°F FOR 3 HOURS. HEATING TO 1750°F FOR ONE HOUR. RAPID QUENCH & SUB ZERO COOL TO -100°F FOR 3 HOURS. HEATING TO 1025°F FOR 3 TO 4 HOURS AND COOLING TO ROOM TEMPERATURE.

II CLOSED DIE FORGING

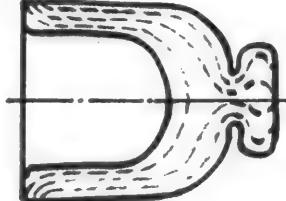
8247-471222-1F



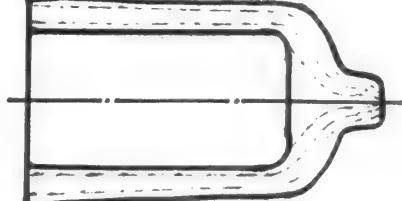
8247-471225-1



8247-471205-1F



8247-471206-1F



A. THE AM355 PARTS ARE CLOSED DIE FORGING WITH CONTROLLED GRAIN FLOW, WITH THE EXCEPTION OF THE 8247-471225-1 STATIONARY HEAD, FUEL TANK. THESE ARE SUPPLIED IN THE EQUALIZED, OVER TEMPERED, AND DESCALDED CONDITION (1425°F, 2 TO 4 HOURS, COOL, 1075°F 2 TO 4 HOURS AND COOL).

B. PRIOR TO ACCEPTANCE, A METALLOGRAPHIC SAMPLE IS CUT FROM EACH FORGING IN THE AS SUPPLIED CONDITION AND HEAT TREATED AS IN ITEM I.D. THE SAMPLES THEN ARE EXAMINED TO DETERMINE THAT THE STRUCTURE IS FREE OF A GRAIN BOUNDARY CARBIDE NETWORK, FREE OF RETAINED AUSTENITE, FREE OF UNTEMPERED MARTENSITE AND THAT THE STRUCTURE DOES NOT CONTAIN MORE THAN 3% DELTA FERRITE AND THAT THE GRAIN SIZE IS AN ASTM 3 OR FINER.

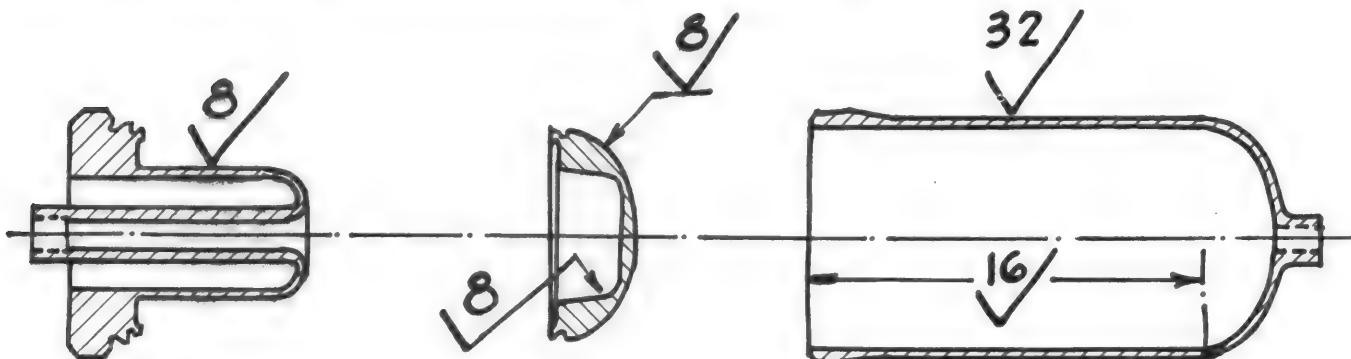
C. THREE HEAT TREATMENT TEST BARS ARE PROVIDED WITH EACH FORGING.

III MACHINED PARTS

A. ROUGH MACHINED PARTS:

THE PARTS ARE ROUGH MACHINED PRIOR TO THE HEAT TREATMENT IN ITEM 1D. THREE TEST BARS ACCOMPANY EACH HEAT TREAT LOAD. AFTER HEAT TREATMENT A SAMPLE IS CUT FROM THE ROUGH MACHINED PART AND EXAMINED METALLURGICALLY AS IN ITEM 2B. THE TEST BARS ARE TESTED FOR CONFORMANCE TO THE MECHANICAL PROPERTIES REQUIRED.

B. FINISH MACHINED PARTS:



FINISHED MACHINED PARTS ARE CLEANED WITH SOLUTIONS THAT ARE CHLORIDE AND FLOURIDE FREE. A PASSIVATING SOLUTION OF INHIBITED NITRIC ACID IS USED FOR THE CHEMICAL CLEANING. THE PARTS ARE TESTED ON THE MASS SPECTROMETER TO A LESS THAN 1×10^{-9} STANDARD CC/SEC OF HELIUM.

MODEL 8247 ACCEPTANCE

TEST PROCEDURE

- I. VISUAL INSPECTION PERFORMED.
- II. WEIGHT TEST.
- III. PROOF TEST.
 - A. GAS SIDE FILL AND VOLUME CALIBRATION
NO BELLOW CYCLING. BELLOW ARE THEN ALLOWED TO GO TO FREE LENGTH AND THE LIQUID SIDE IS FILLED.
 - B. THE TANK IS PROOFTESTED TO 2550 PSIG.
- IV THE TANK IS DRAINED WITHOUT CYCLING THE BELLOW AND THEN THE SHELL IS GAS TESTED TO 1700 PSIG.
- V FLUSHING AND DRYING.
THE TANK IS FLUSHED INTERNALLY WITH DISTILLED WATER AND DRAINED. THE TANK IS THEN DRIED TO AMBIENT DEW POINT.
- VI BELLOW INTEGRITY.
THE BELLOW IS LEAK TESTED AT 15 PSI ΔP EXTENDED. THE BELLOW IS THEN NESTED AND LEAK TESTED AT 15 PSI ΔP AND 150 PSI ΔP .

VII. LUBRICATION APPLICATION.

THE BELLOW IS RETAINED IN A NESTED POSITION WITH VACUUM AND THE TANK IS LUBRICATED. THE LUBRICANT DISTRIBUTION IS THEN PERFORMED BY CYCLING THE BELLOW 22 TIMES IN VARIOUS POSITIONS.

VIII. VOLUME CALIBRATION (LIQUID SIDE).

THE LIQUID SIDE OF THE TANK IS CALIBRATED BY CYCLING 15 TIMES, TO DISPLACE THE AIR IN THE TANK, WITH DISTILLED WATER

IX. FLUSHING AND DRYING.

THE TANK IS FLUSHED ON THE LIQUID SIDE ONLY, WITH FILTERED DISTILLED WATER, THEN DRIED TO A DEW POINT OF -20° F.

X. HANDLING AFTER ACCEPTANCE.

THE AIR VALVES AND PLUGS ARE INSTALLED AND THE GAS SIDE OF THE TANK PRESSURIZED TO 35 PSIG TO RETAIN THE BELLOW IN A NESTED POSITION.

THE TANK IS CHECKED WITH THE DYE PENETRANT METHOD.

THE TANK IS COATED WITH SPRAYLAT FOR HANDLING PROTECTION DURING SUBSEQUENT TESTING.

MODEL 8247 BELLows CORE

I MATERIAL.

THE MATERIAL USED IN THE CORE IS AM 350. THE THICKNESSES USED ARE 0.007" AND 0.014".

II MELTING PRACTICE.

CONSUMABLE ELECTRODE REMELT TECHNIQUE IS PREFERRED, HOWEVER AIRMELTED MATERIAL HAS BEEN ALLOWED THAT COMPLIES WITH ALL THE REQUIREMENTS. (CHEMISTRY, INCLUSIONS, MECHANICAL PROPERTIES).

III HEAT TREATMENT.

THE MATERIAL IS ANNEALLED BY THE REROLLER PRIOR TO FINAL SIZING, BY HEATING TO 1900°F TO 1975°F FOR 15 MINUTES AND THEN QUENCHING.

IV HARDNESS ROCKWELL "C 25" OR LOWER.

THE FORMING, PUNCHING AND WELDING ARE DONE IN THIS CONDITION.

V END DIAPRAGMS.

THE HEAVIER 0.014" END DIAPHRAGMS ARE BLANKED, FORMED, HEAT TREATED AND THEN THE I.D. AND O.D. ARE SIZED.

VI WELDING.

THE CORE IS THEN WELDED COMPLETE WITH HEAVIER END DIAPHRAGMS.

VII HEAT TREATMENT.

THE CORE IS THEN HEAT TREATED IN A RETORT UNDER INERT GAS TO THE SCT 850 CONDITION.
HEAT TO 1710°F FOR 15 MINUTES, RAPID QUENCH TO ROOM $^{\circ}\text{F}$.
COOL TO -100°F FOR 3 HOURS
WARM TO ROOM $^{\circ}\text{F}$
HEAT TO 850°F FOR 3 HOURS
COOL TO ROOM $^{\circ}\text{F}$.

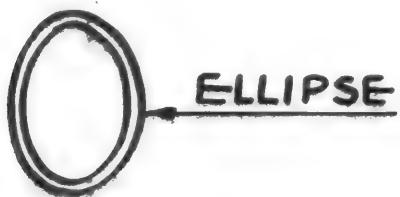
VIII PROBLEMS :

A HIGH REJECTION RATE IS ENCOUNTERED BY THE VENDOR BECAUSE OF WARPING OF THE CORE DURING HEAT TREAT.

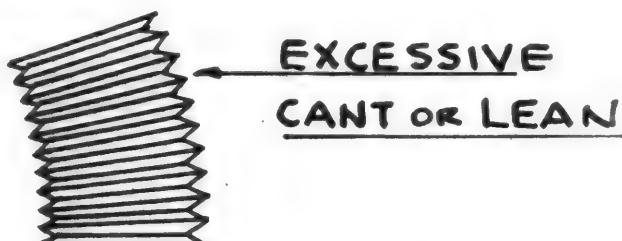
A PARALLEL DEVELOPMENT EFFORT BY THE VENDOR, WITH BELL ASSISTANCE, IS HOPED TO REDUCE THIS REJECTION RATE.

BAC RECOMMENDS HEAT TREATMENT OF BLANKS TO SCT 1025 CONDITION WHICH WILL RESULT IN A ROCKWELL C 35-38. THE FORMING, SIZING & WELDING WILL BE DONE IN THIS CONDITION. THE CORE WILL THEN BE HEAT TREATED TO AN SCT 850 CONDITION AS REQUIRED IN THE BOOK FORM DRAWING.

REJECTIONS :



FAILURE TO PASS PLUG GAUGE



FAILURE TO PASS RING GAUGE

MODEL 8247 START TANKS

<u>DESIGN</u>	<u>IMPROVEMENT</u>	
	<u>001 - 002</u>	<u>201 - 202</u>
HEAT TREATMENT	SCT 850 (AM355)	SCT 1000 (AM355)
GAS FILTER	NO	YES
INSIDE METAL FINISH	RMS 32	RMS 16
MOVEABLE HEAD - - FORGING - CONTOUR - FINISH - MACHINING	FORGED BISCUIT INSIDE CURVE RMS 32 NO GROOVES	CLOSED DIE FORG. INSIDE FLAT RMS 8 VAC. BREAK IN & OUT
BELLOWS ASSY - - CONCENTRICITY - OVALITY CHECK - PLUG GAUGING - SHIPPED - END PLATES	.020 NO NO MECHANICAL NEST .005 TK (OX) .007 TK (FUEL)	.015 YES YES VACUUM NEST .009 TK (OX) .014 TK (FUEL)
STATIONARY HEAD	SAME AS MOVEABLE HEAD	

I DESCRIPTION OF COMP. TESTS.

1. SHOCK

THREE SHOCKS IN EACH DIRECTION ALONG EACH OF THREE MUTUALLY PERPENDICULAR AXES. EACH SHOCK HAVING THE FOLLOWING CHARACTERISTICS: 40G MIN. PEAK ACCEL., 6 MILLISECONDS DURATION AND HAVING AN APPROXIMATE HALF-SINE WAVE FORM.

2. VIBRATION

45 MINUTES ALONG EACH OF THREE MUTUALLY PERPENDICULAR AXES AT A CONSTANT OCTAVE FREQUENCY SWEEP RATE FROM THE LOWER TO THE HIGHER FREQUENCY AT THE FOLLOWING LEVELS:

15 - 40 CPS AT 3.0 G
40 - 400 CPS AT 7.5 G
400 - 3000 CPS AT 20 G

3. ACCELERATION

ACCELERATE FOR 10 MINUTES IN EACH DIRECTION ALONG EACH OF THREE MUTUALLY PERPENDICULAR AXES AT A MIN. OF 12 G'S

4. HI-TEMPERATURE

SOAK FOR 24 HRS. AT +160°F. REDUCE TEMPERATURE TO +140°F. WITH PROPELLANTS AT +140°F CONDUCT 50 CYCLES

5. LO-TEMPERATURE

SOAK FOR 24 HRS. AT -35°F. RAISE TEMPERATURE TO +10°F. WITH PROPELLANTS AT +10°F CONDUCT 50 CYCLES.

6. FLUID RESISTANCE

COMPLETELY FILL TEST UNIT WITH ACTUAL PROPELLANT AND APPLY OPERATING PRESSURE. HOLD IN THIS CONDITION AND MONITOR FOR 30/38 DAYS. DRAIN OFF PROPELLANT AND CALIBRATE WITH TEST PROPELLANT.

7. HUMIDITY

SOAK FOR 360 HRS. AT WET & DRY BULB TEMP. OF +120°F. WITHIN 1 HR. AFTER REMOVING UNIT FROM CHAMBER CONDUCT

1. INSULATION RESISTANCE
2. DIELECTRIC STRENGTH
3. COIL RESISTANCE
4. CALIBRATE

II COMPONENT DEV. TESTS

1. 8247-472-010 FUEL VALVE

1. SHOCK
2. VIBRATION
3. HI-TEMPERATURE
4. ENDURANCE (500 CYCLES)

2. 8247-472-050 OXIDIZER VALVE

1. SHOCK
2. VIBRATION
3. HI-TEMPERATURE
4. ENDURANCE (500 CYCLES)

3. 8247-472-020 FUEL G.G. SOLENOID VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. FLUID RESISTANCE
6. ENDURANCE (2000 CYCLES)
7. HUMIDITY

4. 8247-472-025 OXID. G.G. SOLENOID VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. FLUID RESISTANCE
6. ENDURANCE (2000 CYCLES)
7. HUMIDITY

5. 8247-472-035 OXID. DUAL CR. VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. ENDURANCE (2000 CYCLES)
6. FLUID RESISTANCE

6. 8247-472-040 FUEL DUAL CR. VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. ENDURANCE (2000 CYCLES)
6. FLUID RESISTANCE

7. 8247-472-055 OXID. VENTURI ASSEM.

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. FLUID RESISTANCE

8. 8247-472-060 FUEL VENTURI ASSEM.

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. FLUID RESISTANCE

9. 8247-472-065 OXID. FILL VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. ENDURANCE (1000 CYCLES)
6. FLUID RESISTANCE

10. 8247-472-070 FUEL FILL VALVE

1. SHOCK
2. VIBRATION
3. ACCELERATION
4. HI-LO TEMPERATURE
5. ENDURANCE (1000 CYCLES)
6. FLUID RESISTANCE

11. 8247-472-075 OXID. MANUAL BLEED VALVE

1. DEVELOPED ON MODEL 8101 & RASCAL

12. 8247-472-080 FUEL MANUAL BLEED VALVE

1. DEVELOPED ON MODEL 8101 & RASCAL

13. 8247-472-015 PILOT OPERATED SOLENOID VALVE

1. DEVELOPED ON MODELS 8081 & 8096

14. 8247-472-045 FUEL & OXID. FILTER

1. TESTED WITH FUEL & OXID. VENTURIS

III

DEV. TEST PROBLEMS

1. 8247-472-020-1 FUEL G.G. SOLENOID VALVE

FAILURE: LEAKAGE PAST POPPET UNDER STATIC PRESSURE AT ROOM TEMP.

REMARKS: TEFILON SEAT OF 1 PIECE CONFIGURATION. EFFECTIVE AREA CHG'D UNDER STATIC PRESSURE. REPLACED TEFILON WITH KEL-F. LEAKAGE EXPERIENCED AT HI-TEMPERATURE. REDESIGNED SEAT TO A CONFINED CONFIGURATION USING TEFILON. THIS CHG. CREATED THE 8247-472-020-3 VALVE

2. 8247-472-020-3 FUEL G.G. SOLENOID VALVE

FAILURE: LEAKAGE PAST POPPET DURING VIBRATION.

REMARKS: ADDED PADS TO MOUNTING LUGS TO DAMPEN HIGH FREQUENCIES. THIS CHG. CREATED THE 8247-472-020-5

3. 8247-472-020-5 FUEL G.G. SOLENOID VALVE

FAILURE: BRAZE FAILED ON MOUNTING LUG

REMARKS: REDUCED VIBRATION REQUIREMENTS TO THE FOLLOWING:

25 - 40 CPS AT 5G
40 - 400 CPS AT 7.5G
400 - 2000 CPS AT 15G

THIS CHG. CREATED THE 8247-472-020-7 VALVE.
ALL 8247-472-020-7 VALVES ARE VIBRATED AT
THIS LEVEL NOW.

4. 8247-472-025-1 OXID. G.G. SOLENOID VALVE

FAILURE: LEAKAGE PAST STATIC SEAL
DURING LO-TEMPERATURE SOAK.

REMARKS: STATIC SEAL WAS "K" SEAL AND
TEFLON COATED. TEFLON COATING FOUND PEELING.
ATTEMPTED USING "OMNI" & "RACO" SEALS WITH
NO SUCCESS. PROBLEM WAS SOLVED WITH
"OMEGA" SEAL. THIS CHG. CREATED THE
8247-472-025-3 VALVE.

5. 8247-472-025-3 OXID. G.G. SOLENOID VALVE

FAILURE: HI ΔP DURING CALIB. AT HI TEMPERATURE.

REMARKS: SHANK OF POPPET EXTRUDED INTO OUTLET
FITTING. REDESIGNED POPPET BY INCREASING SHANK
DIAMETER AND CHANGING POINT CONTACT TO CHAMFER
CONTACT. THIS CHG. CREATED THE 8247-472-025-5 VALVE
CHG. ALSO INCLUDED ADDITION OF PADS ON MOUNTING
LUGS.

IV DFT ENGINE PROBLEMS

1. 8247-472-010-3 FUEL VALVE

FAILURE: EXCESSIVE LEAKAGE PAST SLIPPER SEALS.

REMARKS: VALVE WAS CALIBRATED AFTER ENGINE TESTS. DATA WITHIN SPECIFICATION. FAILED FINAL LEAKAGE TESTS. "O" RINGS HAD TAKEN A SET AND LOST THEIR DUROMETER. SIMILAR VALVE ON THE XRM-3 ENGINE DEMONSTRATED 45 SUCCESSFUL FIRINGS WITH NO PROBLEMS. INVESTIGATING NEW "O" RING MATERIAL ON MODEL 8096.

2. 8247-472-025-3 OXID. G.G. SOLENOID VALVE

FAILURE: VALVE REMOVED FROM ENGINE TO BE REWORKED INTO A -5 CONFIGURATION. CORROSION FOUND INSIDE OF VALVE.

REMARKS: ENCAPSULATION COPPER BRAZED. MACHINING OF ENCAPSULATION NOT CLOSELY CONTROLLED. RESULT. COPPER PENETRATION & PIN HOLES IN ENCAPSULATION ATTACKED BY ACID. CHANGED COPPER BRAZE TO GOLD-NICKEL BRAZE (LESS PENETRATION). ESTABLISHED TIGHTER CONTROL ON ENCAPSULATION MACHINING. THIS CHG. CREATED THE 8247-472-025-7 VALVE FOR FLIGHT VERIFICATION TESTS.

3. 8247-472-040-1 FUEL DUAL CH. VALVE

FAILURE: LEAKAGE PAST INLET POPPET

REMARKS: VALVE LEAKED AFTER HUMIDITY TEST. SEAT ON INLET POPPET FOUND OUT OF ITS GROOVE. CAUSE - HI. VELOCITY. SOURCE UNKNOWN. REDESIGNED SEAT TO A DOVETAIL CONFIGURATION. THIS CHANGE CREATED THE 8247-472-040-3 VALVE AND THE 8247-472-035-3 VALVE FOR FLIGHT VERIFICATION TESTS. IN ACCEPTANCE TESTS OF THE 8247-472-040-3 VALVE THE ΔP WAS OUT OF SPECIFICATION. IN THE REDESIGN THE POPPET HAD BEEN MADE LONGER. THE POPPET WAS SHORTENED AND THE OUTLET POPPET SPRING RETAINER WAS REDESIGNED TO PREVENT COCKING. THIS CHANGE NOW CREATED THE 8247-472-040-5 FOR FLIGHT VERIFICATION TESTS.

VI FLIGHT VERIFICATION TESTS

1. 8247-472-035-3 OXID. DUAL CK. VALVE

1. SHOCK
2. VIBRATION
3. HI-LO TEMPERATURE
4. ENDURANCE (2000 CYCLES)

2. 8247-472-035-3 OXID. DUAL CK. VALVE

1. SHOCK
2. VIBRATION
3. HI-LO TEMPERATURE
4. 38 DAY STORAGE TEST ON START TANK SYSTEM.

3. 8247-472-040-5 FUEL DUAL CK. VALVE

1. HI-LO TEMPERATURE
2. SHOCK
3. VIBRATION
4. ENDURANCE (2000 CYCLES)

4. 8247-472-040-5 FUEL DUAL CK. VALVE

1. HI-LO TEMPERATURE
2. SHOCK
3. VIBRATION
4. 38 DAY STORAGE TEST ON START TANK SYSTEM.

5. 8247-472-025-7 OXID.G.G. SOLENOID VALVE

1. SHOCK
2. VIBRATION
3. HI-LO TEMPERATURE
4. 38 DAY STORAGE TEST ON START TANK SYSTEM.

6. 8247-472-025-7 OXID.G.G. SOLENOID VALVE

1. HI-LO TEMPERATURE
2. SHOCK
3. VIBRATION
4. ENDURANCE (2000 CYCLES)

7. 8247-472-020-7 FUEL G.G. SOLENOID VALVE

1. EXPLOSION PROOF
 - A. SEA LEVEL - 5000 FT (10 CYCLES)
 - B. AT 10,000 FT. (10 CYCLES)
2. ALTITUDE TEST
 - A. 90,000-100,000 FT. AT .2 PSIA (100 CYCLES)

8. 8247-472-025-7 OXID.G.G. SOLENOID VALVE

1. EXPLOSION PROOF
 - A. SEA LEVEL - 5000 FT (10 CYCLES)
 - B. AT 10,000 FT. (10 CYCLES)
2. ALTITUDE TEST
 - A. 90,000-100,000 FT. AT .2 PSIA (100 CYCLES)

VI FLIGHT VER. TEST PROBLEMS

1. 8247-472-025-7 OXID. G.G. SOLENOID VALVE

FAILURE: HI DO DURING CALIB AT HI-TEMP.
FOLLOWING DYNAMIC TESTS.

REMARKS: SHOULDER ON POPPET FOUND
DEFORMED. POPPET LIFT INCREASED FROM .006/.008
TO .014. STRESS LEVEL ON SHOULDER MARGINAL.
SHOULDER WAS NOT INCREASED, WHEN SHANK WAS
INCREASED DURING DEVELOPMENT TESTS, TO
MAINTAIN SAME STRESS LEVEL. REDESIGNED
POPPET TO INCREASE SHOULDER BEARING AREA.
THIS CHANGE CREATED 8247-472-025-9 VALVE
FOR RE-RUN OF FLIGHT VERIFICATION TESTS.

ELECTRICAL CHARACTERISTICS OF MODEL 8247 COMPONENTS

<u>GAS GEN. FUEL SOLENOID VALVE 8247 - 472 020</u>				
<u>INSULATION RESISTANCE</u>	-	AT ROOM AMBIENT & 500 VDC AT EXTREME TEMP., HUMIDITY, ALTITUDE & 500 VDC	= 500 MEGOHMS	
<u>DIELECTRIC STRENGTH</u>	-	AT SEA LEVEL, 1000 VAC RMS 60 CPS AT EXTREME TEMP., HUMIDITY, ALTITUDE & 1000 VAC RMS 60 CPS	= 50 MEGOHMS = 0.5 M AMPS	
<u>COIL RESISTANCE</u>	-	AT 70°F	= 2.0 M AMPS	
<u>CURRENT PULL-IN VOLTAGE</u>	-	AT 70°F SEA LEVEL & 30.5 VDC	= 8.5 ± 0.3 OHMMS = 3.72 AMPS MAX	
<u>PULL-OUT VOLTAGE</u>	-	-	= 18 VDC = 2.5 VDC	
<u>GAS GEN. OXIDIZER SOLENOID VALVE 8247 - 472 025</u>				
<u>INSULATION RESISTANCE</u>	-	AT ROOM AMBIENT & 500 VDC AT EXTREME TEMP., HUMIDITY, ALTITUDE & 500 VDC	= 500 MEGOHMS	
<u>DIELECTRIC STRENGTH</u>	-	AT SEA LEVEL, 1000 VAC RMS 60 CPS AT EXTREME TEMP., HUMIDITY, ALTITUDE & 1000 VAC RMS 60 CPS	= 50 MEGOHMS = 0.5 M AMPS	
<u>COIL RESISTANCE</u>	-	AT 70°F	= 2.0 M AMPS	
<u>CURRENT PULL-IN VOLTAGE</u>	-	AT 70°F SEA LEVEL & 30.5 VDC	= 16.7 ± 0.5 OHMMS = 1.88 AMPS MAX	
<u>PULL-OUT VOLTAGE</u>	-	-	= 18 VDC = 2.5 VDC	
<u>PILOT OPERATED SOLENOID VALVE 8247 - 472 015</u>				
<u>INSULATION RESISTANCE</u>	-	AT ROOM AMBIENT & 500 VDC AT SEA LEVEL, 600 VAC RMS 60 CPS AT $80^{\circ}\text{F} \pm 20^{\circ}\text{F}$	= 500 MEGOHMS = 0.5 M AMPS = 12.5 ± 0.5 OHMMS	

MOTIONAL PICKUP TRANSDUCER (8247-472084-3)

CHARACTERISTICS

VOLTAGE AMPLITUDE - 1.4 TO 5V PEAK TO PEAK

(DEPENDING ON AIR GAP SETTING)

$$\text{CONVERSION FACTOR} - \frac{\text{PEAK TO PEAK VOLTAGE}}{2.828} = \text{RMS VOLTAGE}$$

WAVE FORM - (BY HARMONIC ANALYSIS)

MODIFIED FULL SINE WAVE FORM

SECOND - HARMONIC	60 % OF FUNDAMENTAL
THIRD - HARMONIC	2 % OF FUNDAMENTAL
FOURTH - HARMONIC	10 % OF FUNDAMENTAL
FIFTH - HARMONIC	0 % OF FUNDAMENTAL

FREQUENCY - 958 CPS CORRESPONDING TO ENGINE SPEED OF 24,800 RPM

MAX. ACCELERATION - 1940 CPS^2 CORRESPONDING TO THEORETICAL $\frac{dn}{dt}$ OF 50,000 RPM/SEC WITH DRY PUMP AND BOTH START TANKS FULLY LOADED AND PRESSURIZED

DC RESISTANCE - $57.5 \pm 2.5 \text{ OHMSS}$

AC IMPEDANCE - 100 OHMSS NOMINAL AT 1000 CPS

ELECTRONIC GATE (8247-472283-3)

PURPOSE:

- A. PROVIDE OVERSPEED SHUT-DOWN CAPABILITY
- B. JUNCTION POINT FOR POWER TO ENGINE SOLENOIDS

INPUT SIGNAL REQUIREMENTS

- AMPLITUDE - 1.4 TO 5.0V PEAK TO PEAK (SPEC)
1V PEAK TO PEAK (MINIMUM ACTUAL)
- WAVEFORM - NOT AFFECTED BY HARMONIC CONTENT
OF SIGNAL
- FREQUENCY - 0 TO 2800 CPS
- INSTRUMENTATION TRANSFORMER OUTPUT - 60%
OF INPUT AMPLITUDE
- TRIP FREQUENCY - 1140 ± 20 CPS (ALL CONDITIONS)
- TRIP FREQUENCY BANDWIDTH - 250 ± 50 CPS

ELECTRONIC GATE (8247-472283-3)

POWER INPUT -

VOLTAGE 19.5 TO 30.5 VDC, 500 MV RIPPLE
POWER (ELECTRONIC CIRCUITS). 1A AT 28 VDC
VOLTAGE DROP (GATE) 1 VDC @ 19.5V AND RATED LOAD
1.25 VDC @ 30.5V AND RATED LOAD
VOLTAGE DROP (TOTAL - INCLUDING 4 FEET OF WIRE)
1.4 VDC @ 19.5V AND RATED LOAD
1.85 VDC @ 30.5V AND RATED LOAD

LINE VOLTAGE TRANSIENT - NO EFFECT

CIRCUIT PROTECTION - POLARITY REVERSAL DIODES

PART FAILURE - DESIGN OBJECTIVE - THAT A SINGLE PART FAILURE
DOES NOT LATCH THE RELAYS

RESET CIRCUIT - 19.5 TO 30.5 VDC 500 MV RIPPLE TO RELAY RESET COILS

ELECTRONIC GATE (8247-472283-3)

ACCEPTANCE TEST (100%)

RELAY ONLY

VIBRATION - 5 TO 45 CPS AT .3 IN DA
45 TO 3000 CPS AT 30 G
CYCLES - 2000 CYCLES AT 25°C
2000 CYCLES AT -65°C
2000 CYCLES AT +125°C

COMPONENT

INSULATION RESISTANCE (500 MEGOHM AT 500 VDC)
CONTINUITY (SIMPSON MODEL 260)
LINE TRANSIENT (200 TO 300 VOLT NEG SPIKE)
TRIP FREQUENCY (ROOM TEMPERATURE, 0°F + 160°F)
TRIP FREQUENCY BAND WIDTH (ROOM TEMPERATURE, 0°F + 60°F)
SHOCK - 40G (MINIMUM)
VIBRATION - 25 TO 2000 CPS AT 5G

ELECTRONIC GATE 8247-472283 TESTS

R E D

I. REFERENCE TEST

- (a) LINE TRANSIENT
- (b) BANDWIDTH AND SENSITIVITY
- (c) INSULATION RESISTANCE
- (d) RESISTANCE AND CONTINUITY

LOW (-65°F TO 0°F) & HIGH (+200°F TO +160°F) TEMP.

2. TEMP. SHOCK (+185°F TO -40°F)

3. EMI (MIL-I-26600 & 8247-947006)

4. HUMIDITY

5. SALT SPRAY

6. SHOCK

7. ACCELERATION

8. SINUSOIDAL VIBRATION (3000 CPS, 5 TO 20 G)

9. RANDOM VIBRATION

10. RANDOM VIBRATION

PFRT

- 1. ALTITUDE (0.2 PSIA MIN)
- 2. IGNITION PROOF

CABLE ASSY (8247-472291-1)

CONNECTORS - DEUTSCH CO. EXCEPT FOR PILOT OPERATED
SOL VALVE (TITEFLEX)
22005 (~DTK07) - SINGLE MOUNTING HOLE
22007 (~DTK06) - PLUG

WIRE - MIL-W-16878
TEFLON INSULATED, GA - 20
TWISTED & SHIELDED

ROUTING - CONTROL WIRING ROUTED
SEPARATE FROM INSTRUMENTATION

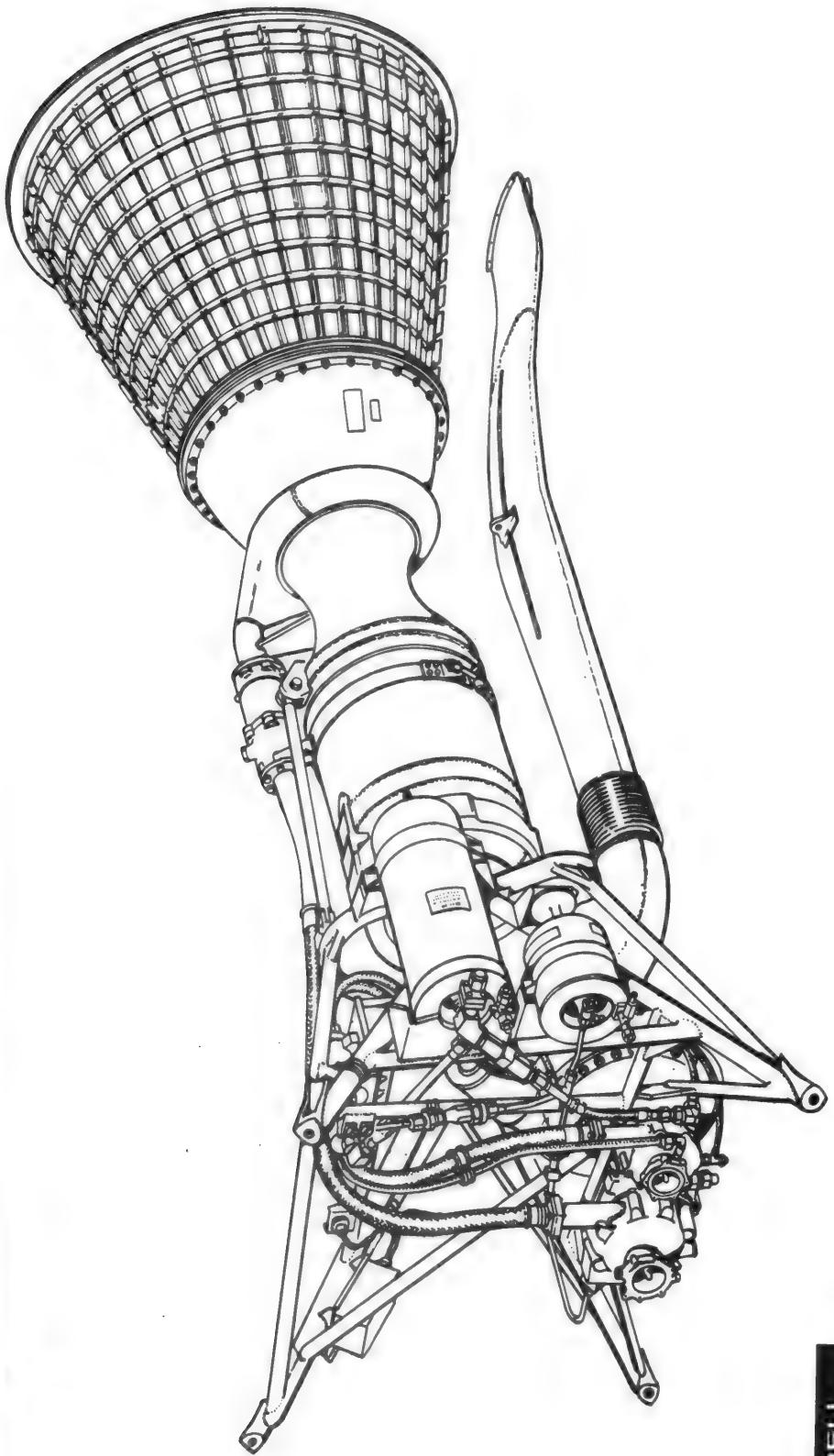
REPAIR - SPECIAL TOOLS REQ'D

ACCEPTANCE TEST - CONTINUITY
DIELECTRIC STRENGTH - 600 V RMS
INSULATION RESISTANCE - 500 V DC

CABLE CLAMPS - THOMAS ASSOC. TYPE TA73255 & TA713D SERIES - T 4B TY5 SERIES

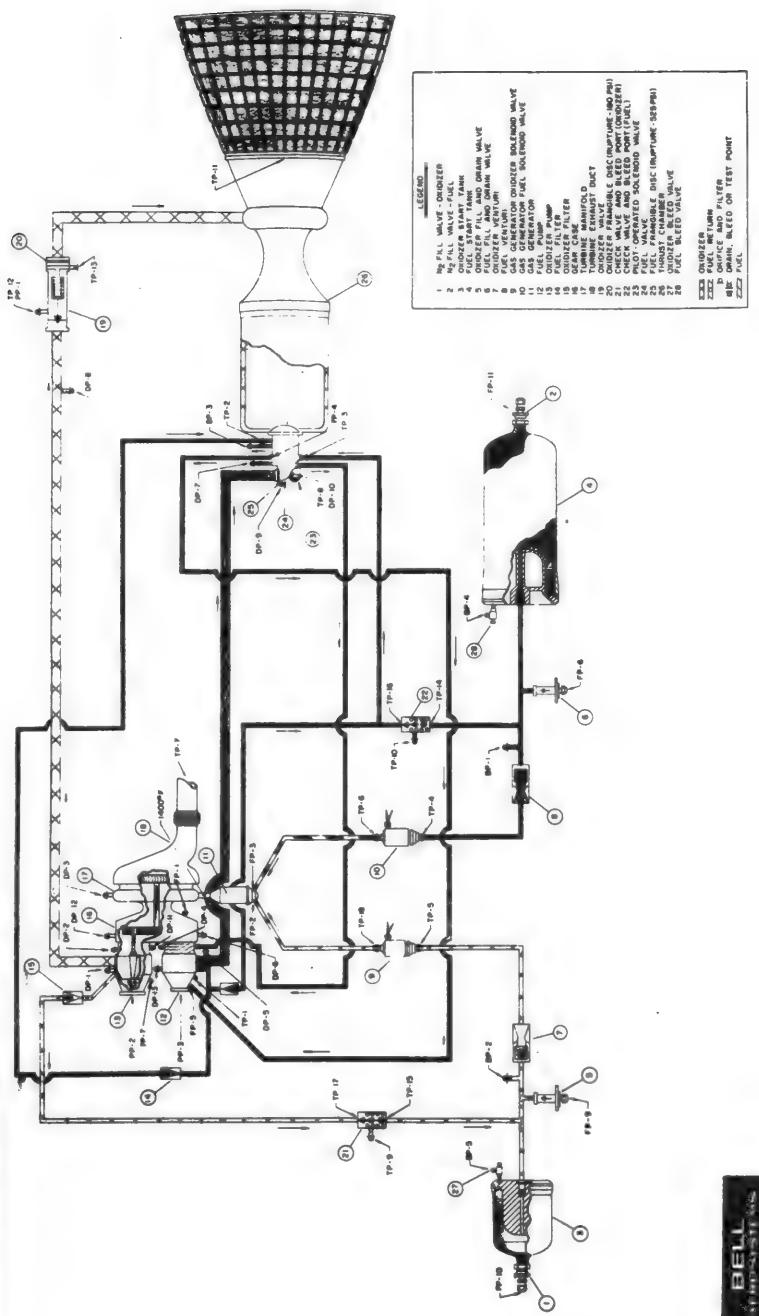
Model 8247

ENGINE ASSEMBLY



Model 8247

ROCKET ENGINE - PROPELLANT FLOW



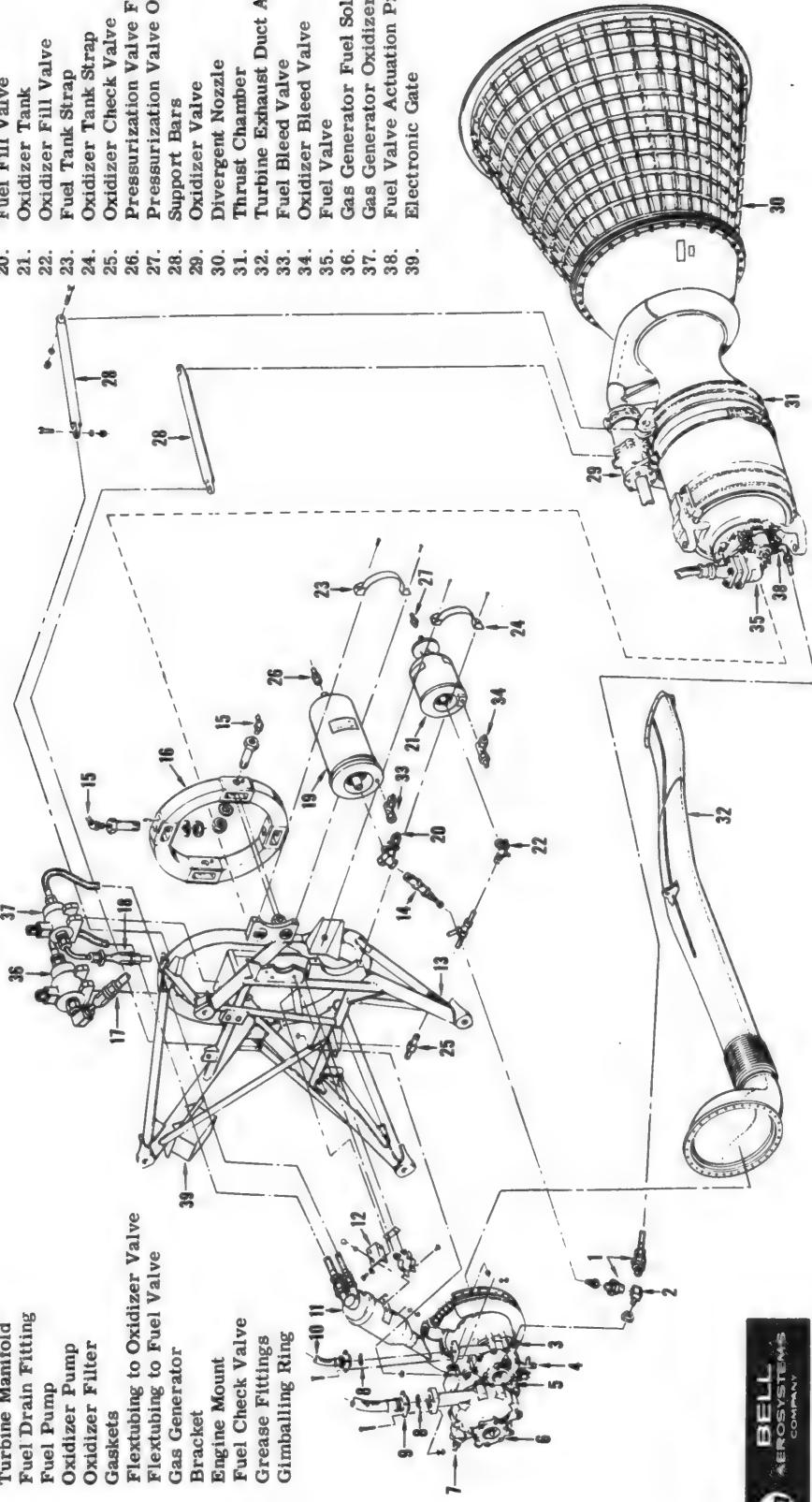
BELL
TELEVISION

Model 8247

ENGINE COMPONENTS

1. Fuel Filter
2. Elbow
3. Turbine Manifold
4. Fuel Drain Fitting
5. Fuel Pump
6. Oxidizer Pump
7. Oxidizer Filter
8. Gaskets
9. Flextubing to Oxidizer Valve
10. Flextubing to Fuel Valve
11. Gas Generator
12. Bracket
13. Engine Mount
14. Fuel Check Valve
15. Grease Fittings
16. Gimbal Ring

17. Fuel Filtered Venturi
18. Oxidizer Filtered Venturi
19. Fuel Tank
20. Fuel Fill Valve
21. Oxidizer Tank
22. Oxidizer Fill Valve
23. Fuel Tank Strap
24. Oxidizer Tank Strap
25. Oxidizer Check Valve
26. Pressurization Valve Fuel
27. Pressurization Valve Oxidize
28. Support Bars
29. Oxidizer Valve
30. Divergent Nozzle
31. Thrust Chamber
32. Turbine Exhaust Duct Agena
33. Fuel Bleed Valve
34. Oxidizer Bleed Valve
35. Fuel Valve
36. Gas Generator Fuel Solenoid
37. Gas Generator Oxidizer Solen
38. Fuel Valve Actuation Pressure
39. Electronic Gate

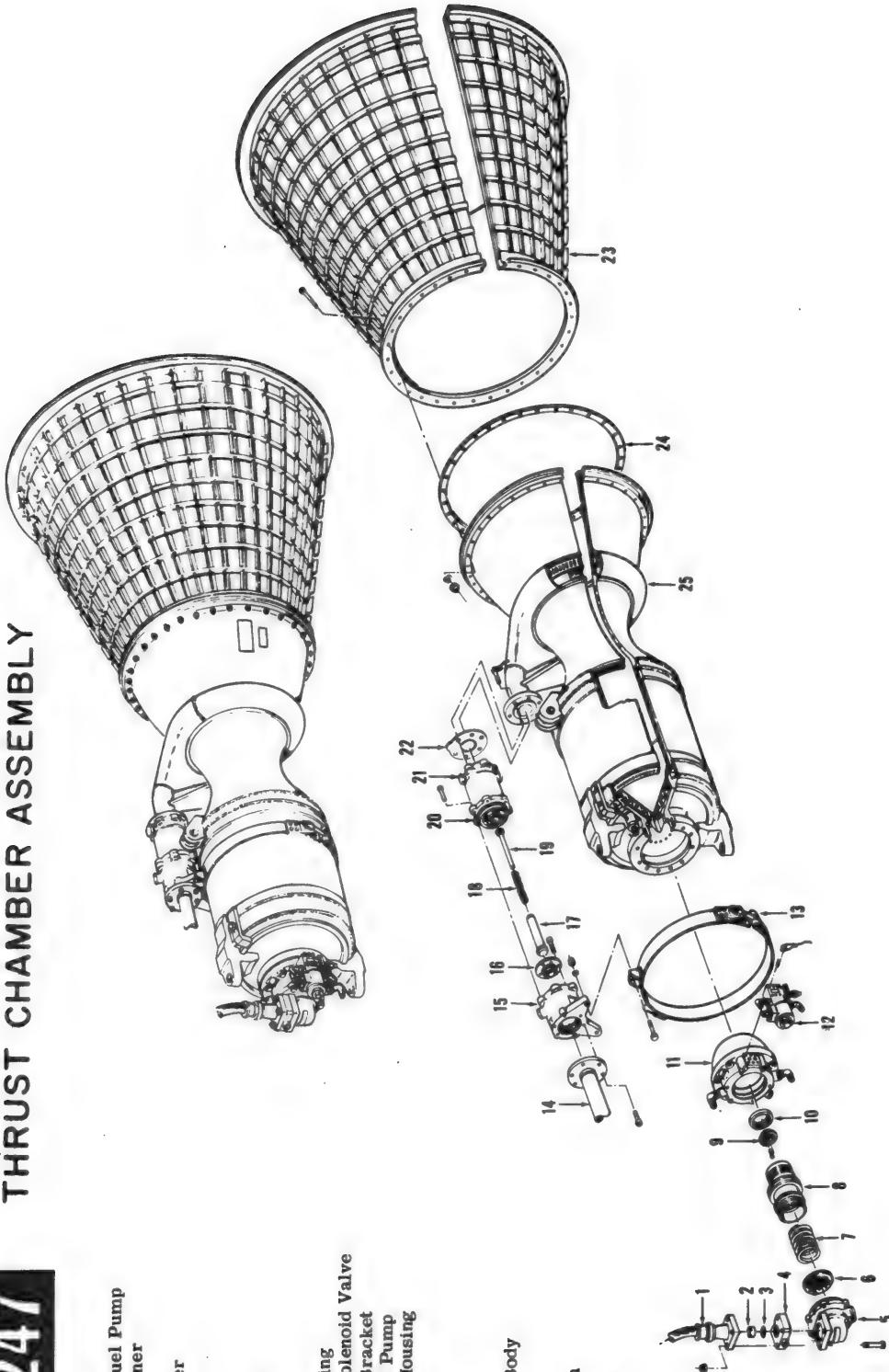


BELL EROSYSTEMS
COMPANY

Model 8247

THRUST CHAMBER ASSEMBLY

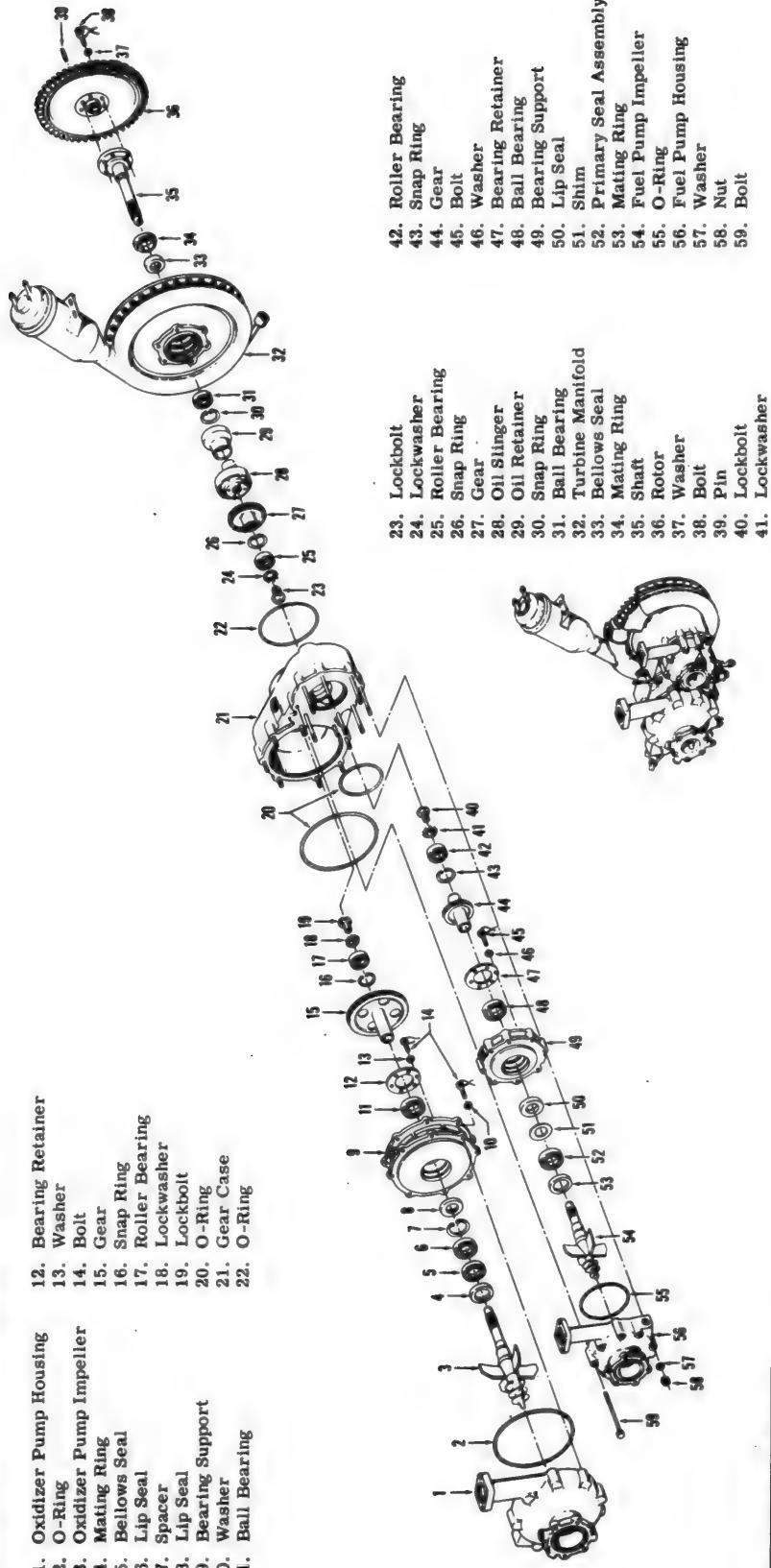
1. Flex Tubing to Fuel Pump
2. Burst Disc Retainer
3. Burst Disc
4. Burst Disc Holder
5. Elbow
6. Screen
7. Spring
8. Actuating Piston
9. Retainer
10. Seat
11. Fuel Valve Housing
12. Pilot Operated Solenoid Valve
13. Oxidizer Valve Bracket
14. Tube to Oxidizer Pump
15. Oxidizer Valve Housing
16. Seat Assembly
17. Poppet
18. Spring
19. Spring Guide
20. Oxidizer Valve Body
21. Vent Fitting
22. Burst Disc
23. Nozzle Extension
24. Gasket
25. Thrust Chamber



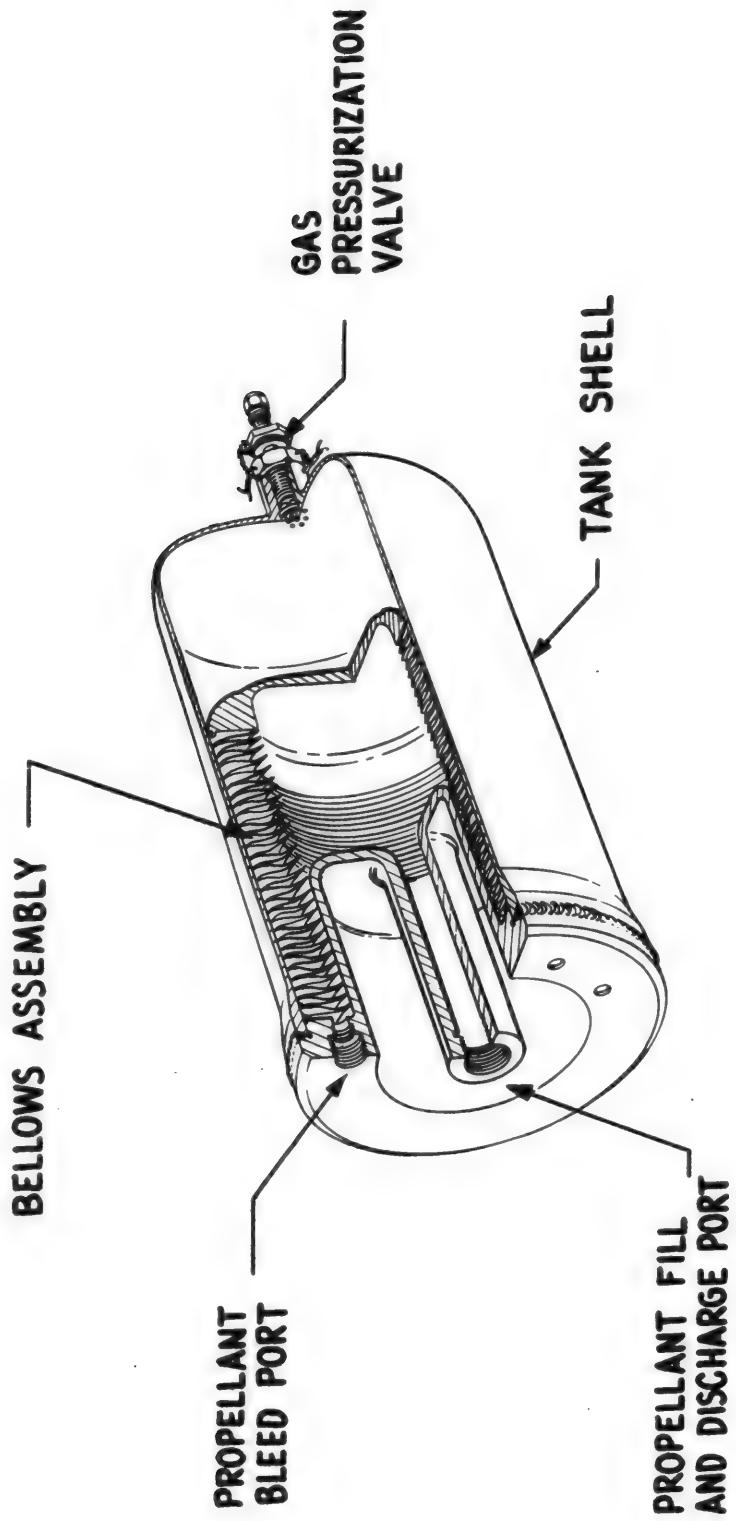
Model 8247

TURBINE PUMP ASSEMBLY

1. Oxidizer Pump Housing
2. O-Ring
3. Oxidizer Pump Impeller
4. Mating Ring
5. Bellows Seal
6. Lip Seal
7. Spacer
8. Lip Seal
9. Bearing Support
10. Washer
11. Ball Bearing
12. Bearing Retainer
13. Washer
14. Bolt
15. Gear
16. Snap Ring
17. Roller Bearing
18. Lockwasher
19. Lockbolt
20. O-Ring
21. Gear Case
22. O-Ring



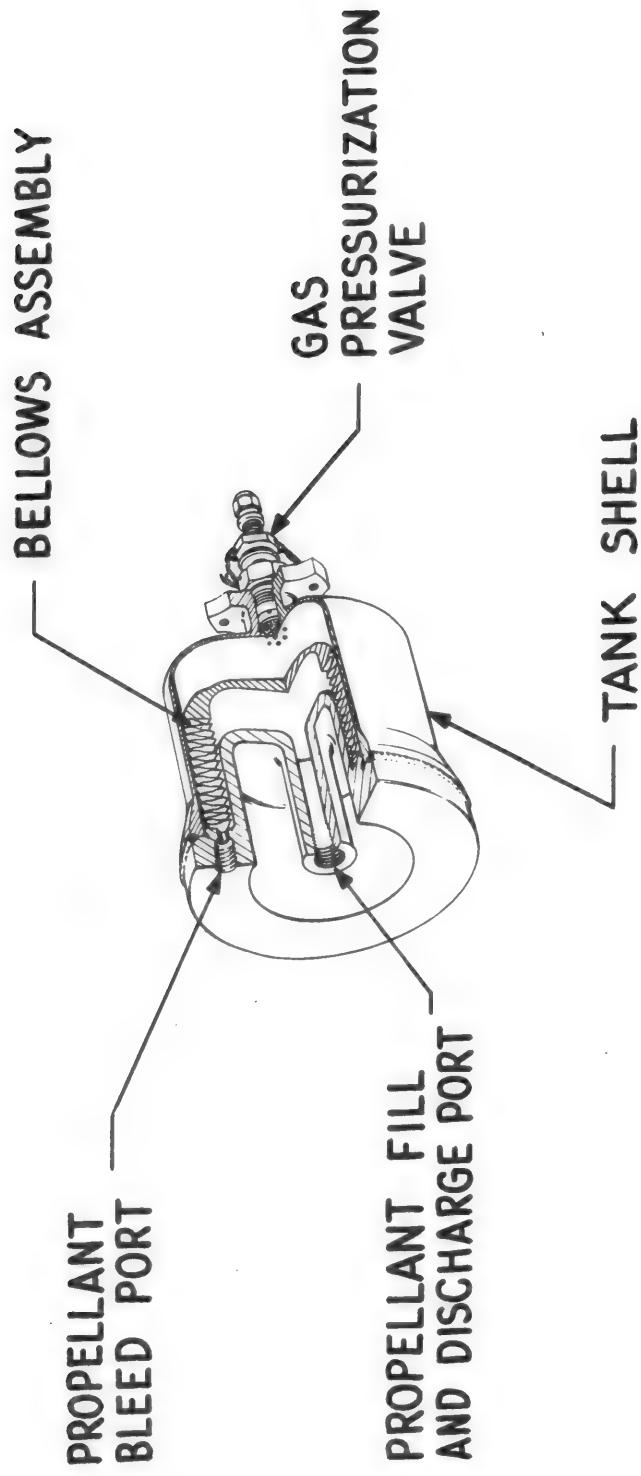
START TANK - FUEL



b
BELL
AEROSYSTEMS
COMPANY

8247-471202

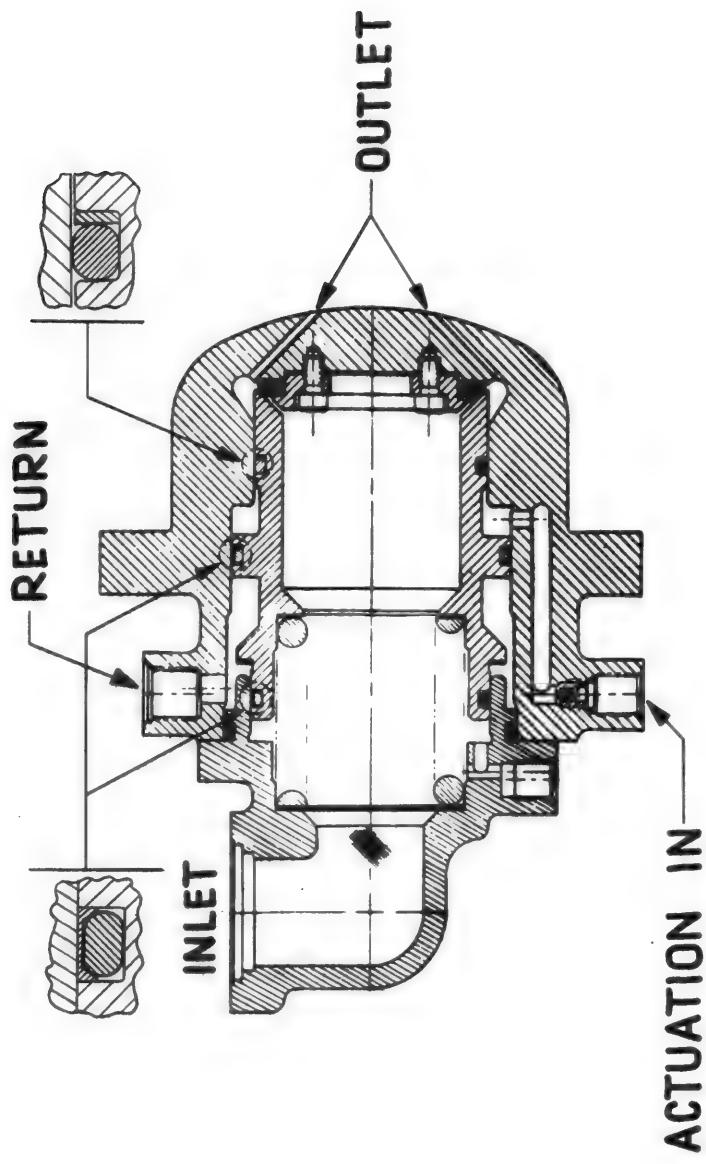
START TANK-OXIDIZER



BELL
AEROSYSTEMS
COMPANY

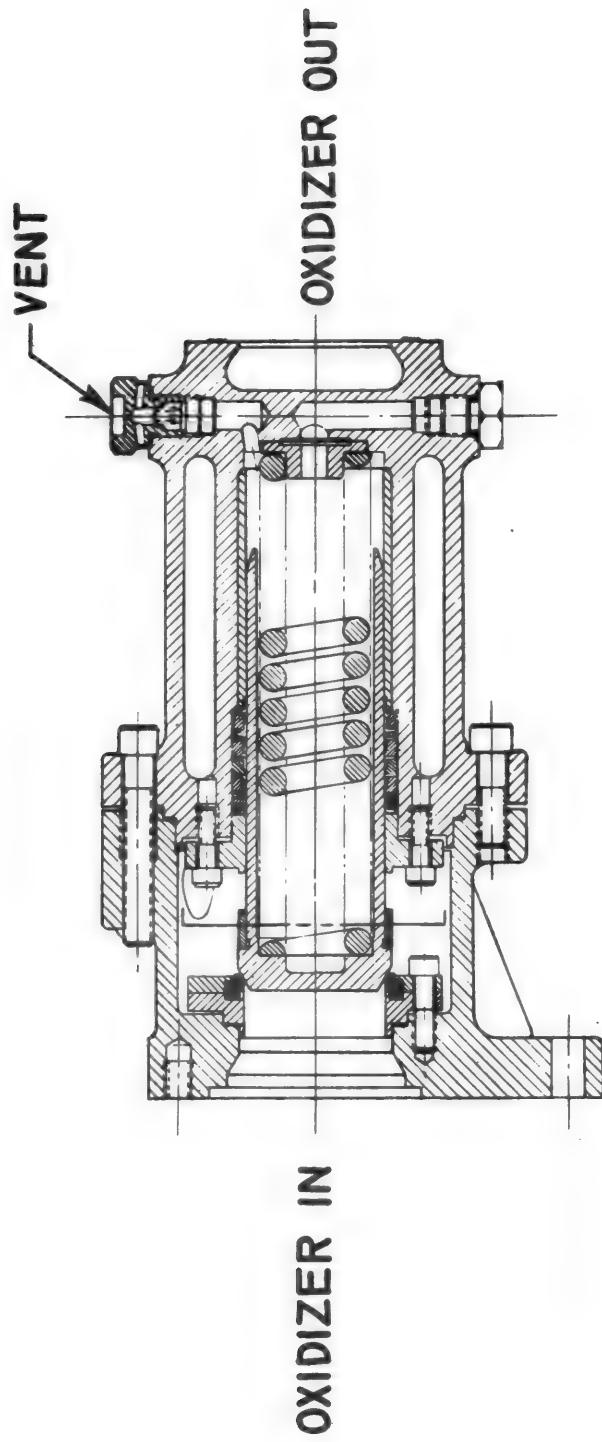
8247-471201-1

FUEL VALVE



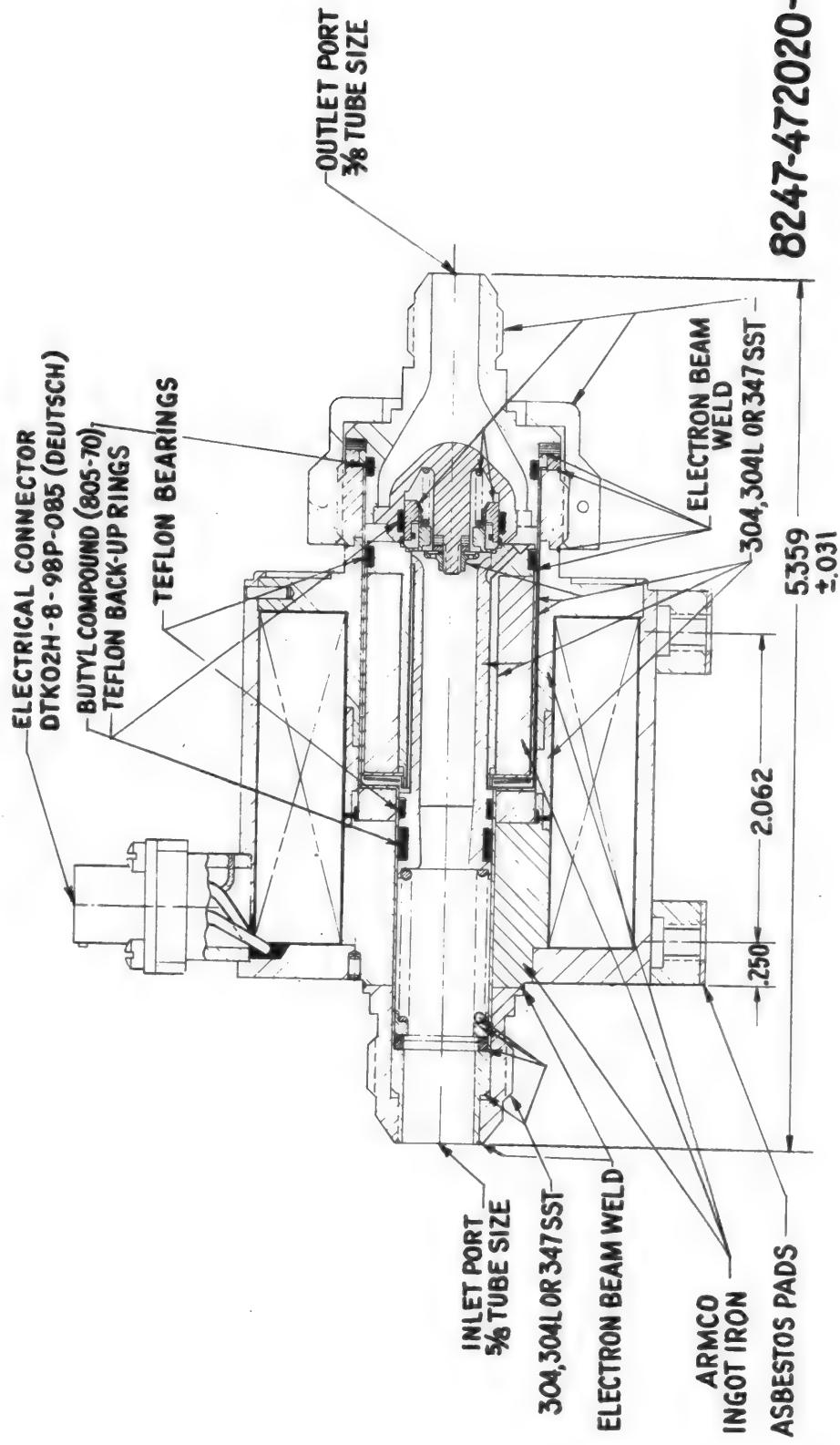
8247-472010-3

OXIDIZER VALVE

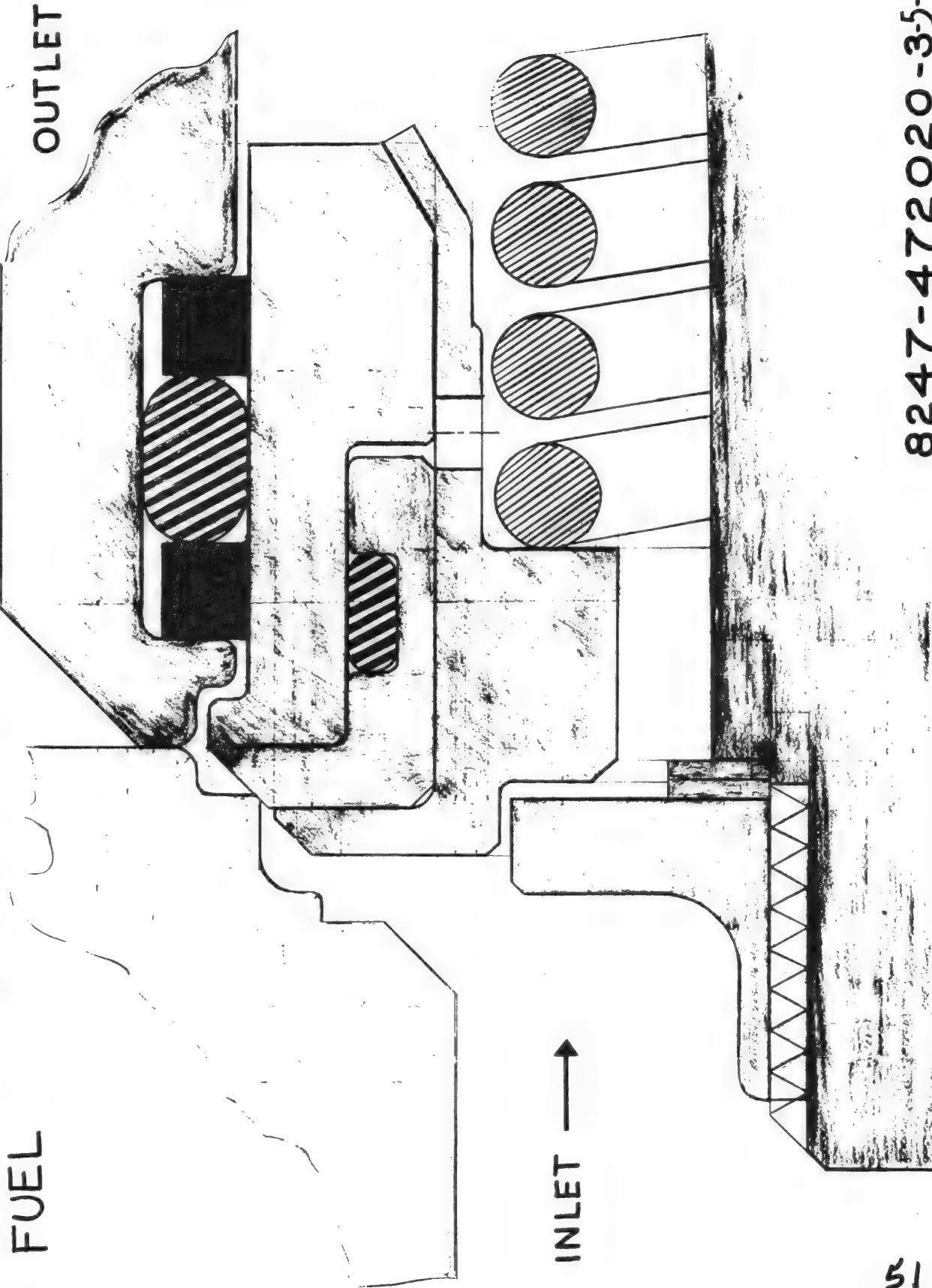


8427-472050-1

GAS GENERATOR FUEL SOLENOID VALVE



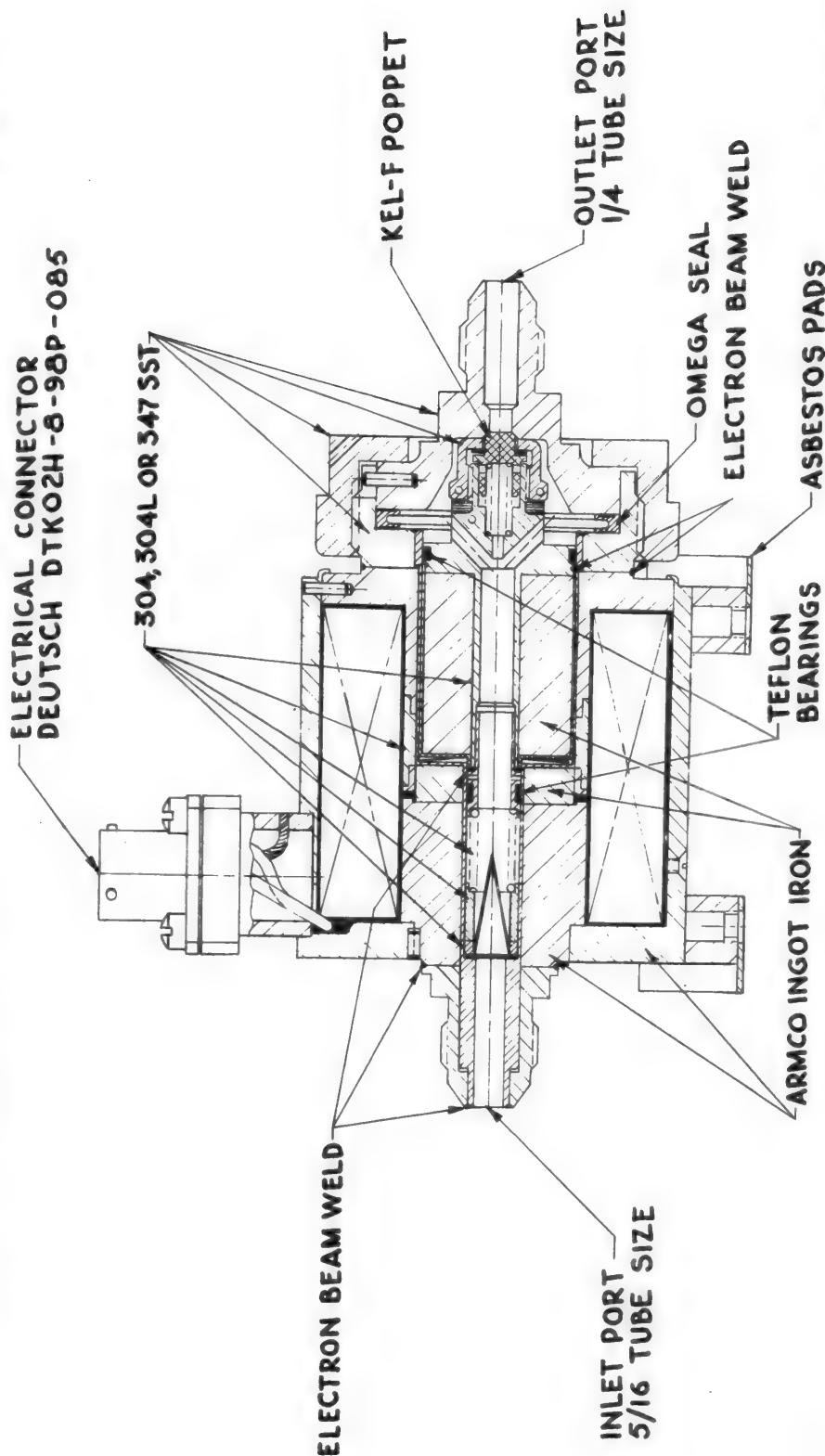
GAS GENERATOR SOLENOID VALVE



51

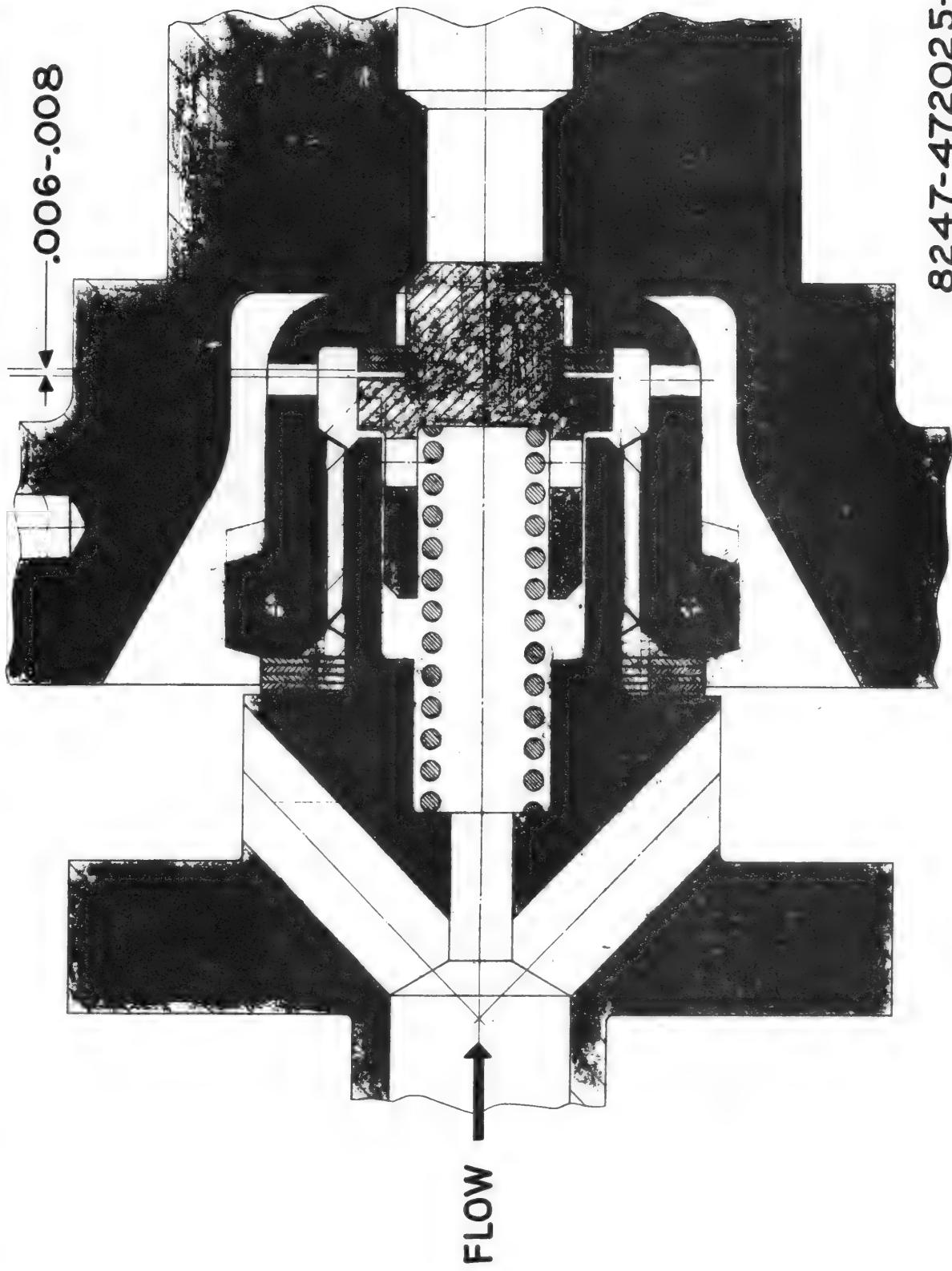
8247-472020-357

GAS GENERATOR OXIDIZER SOLENOID VALVE



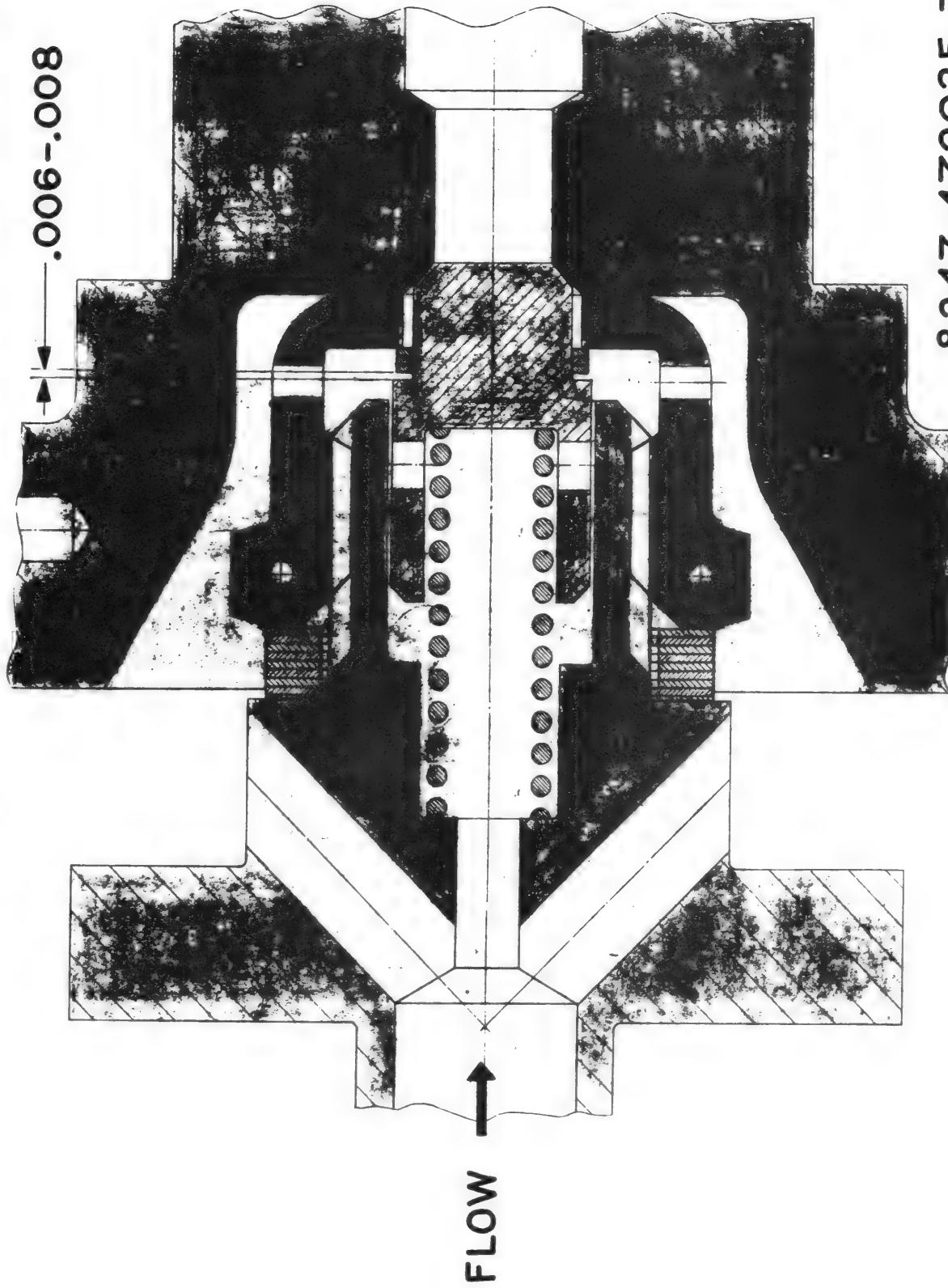
GAS GENERATOR OXIDIZER SOLENOID VALVE

.006-.008

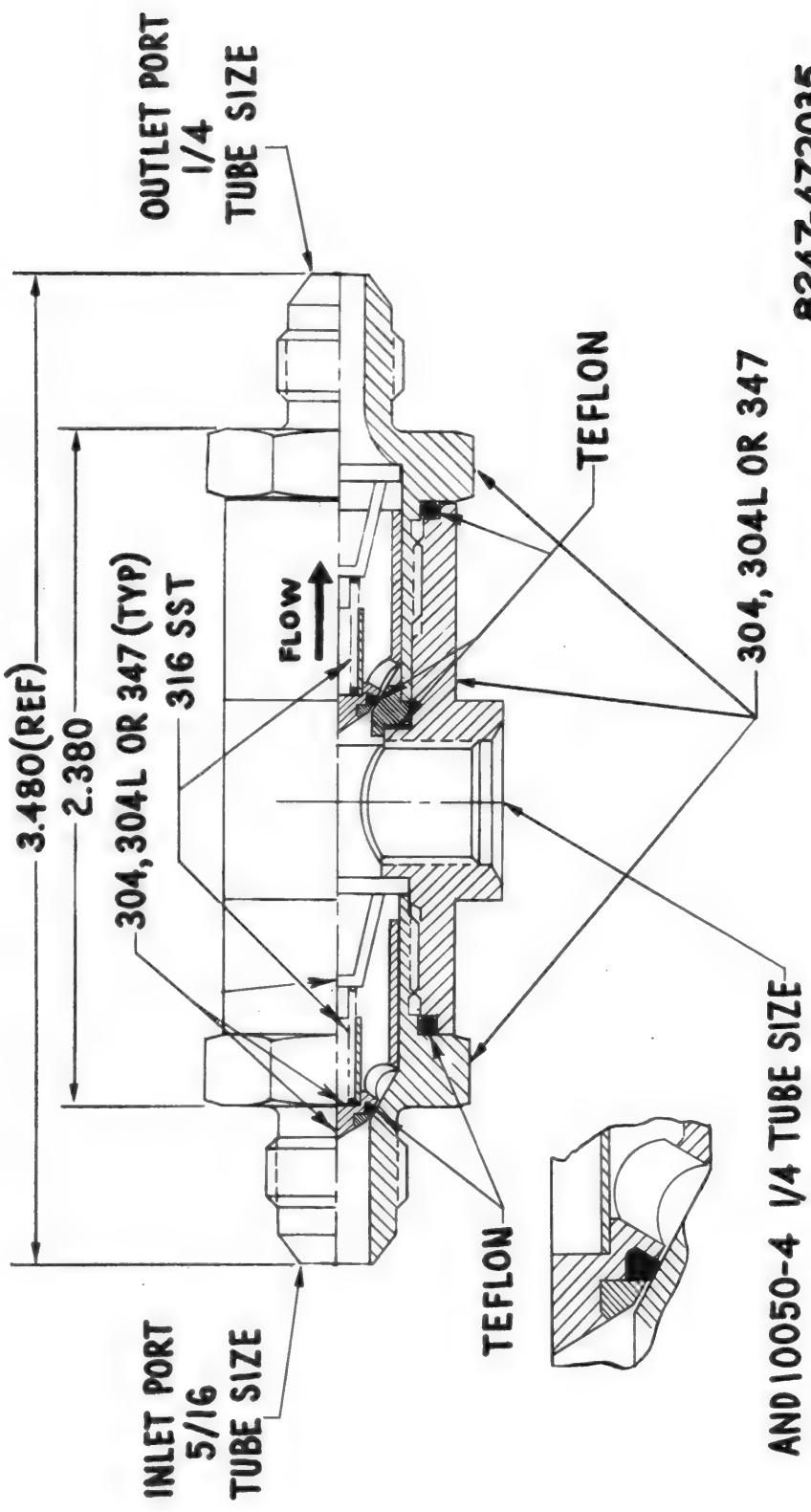


GAS GENERATOR OXIDIZER SOLENOID VALVE

.006-.008



OXIDIZER DUAL-CHECK VALVE

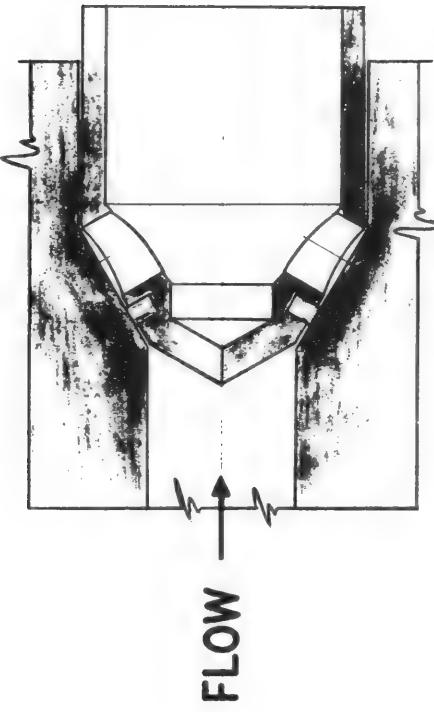


8247-472035

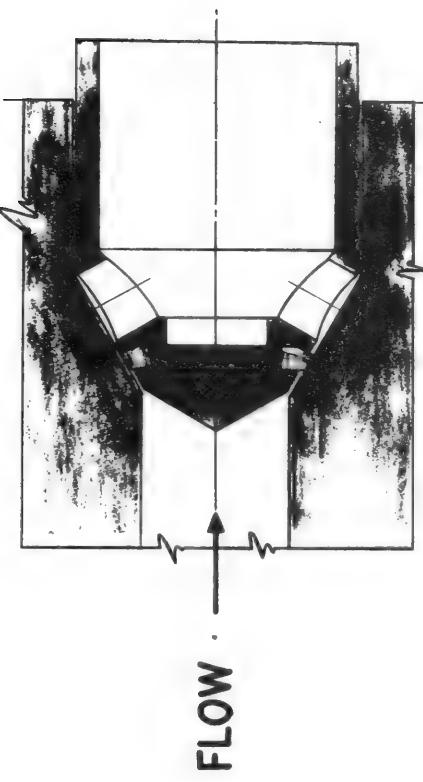
AND 10050-4 $\frac{1}{4}$ TUBE SIZE

55

OXIDIZER DUAL CHECK VALVE

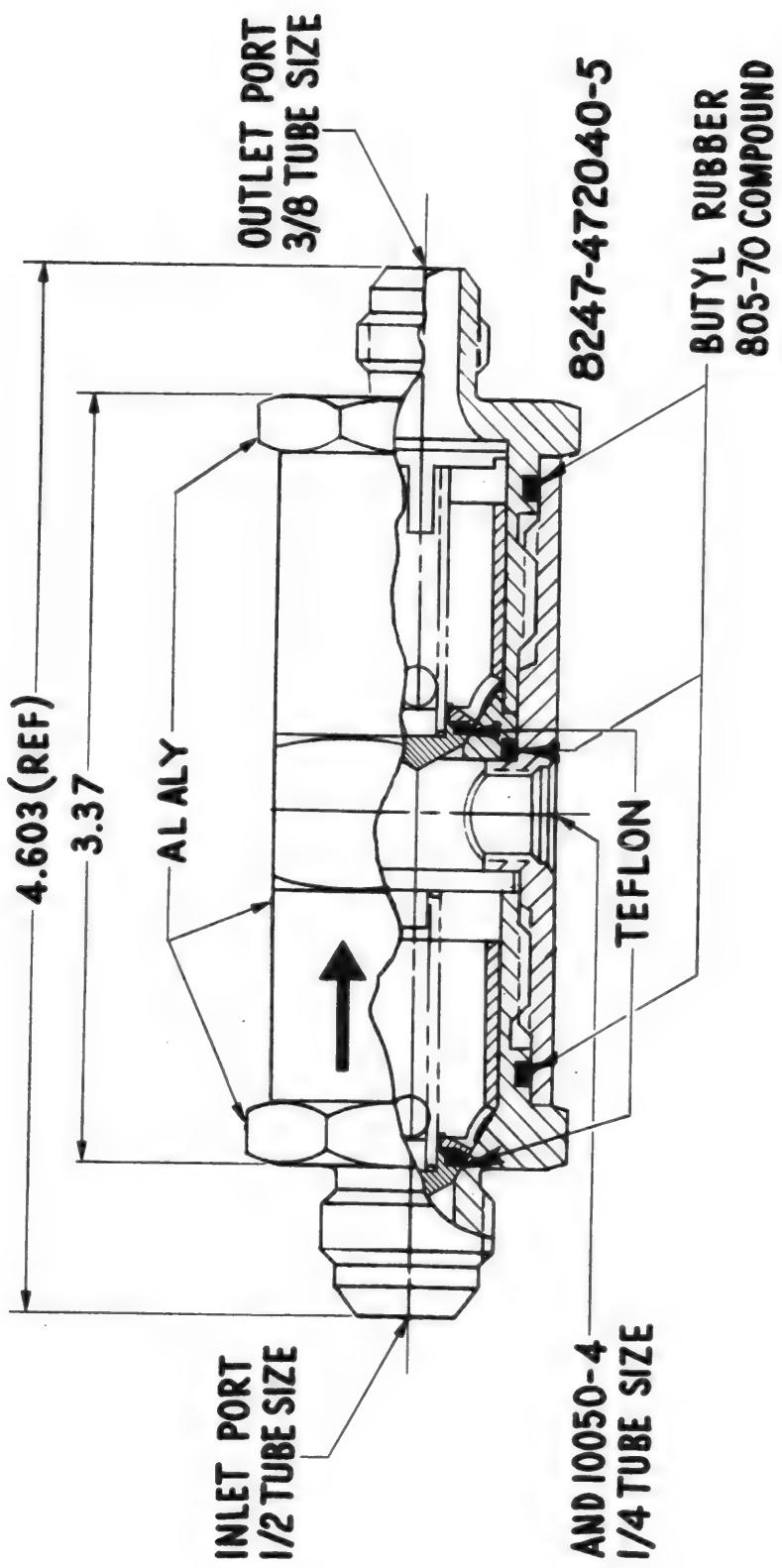


8247-472-035-1

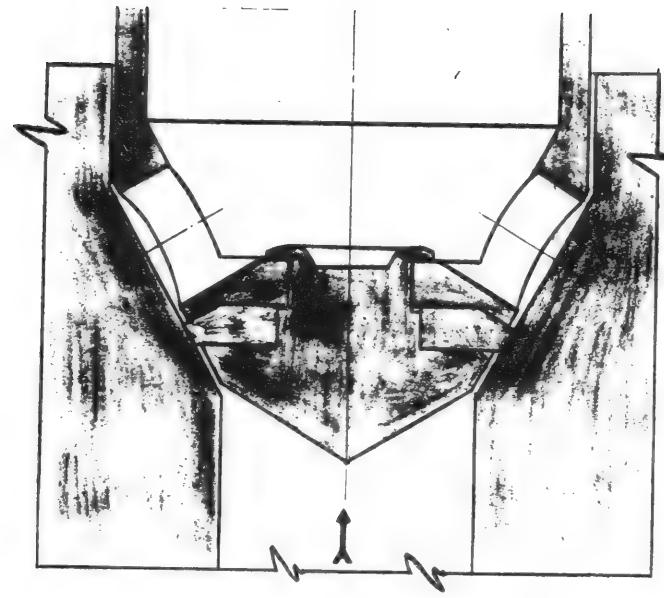


8247-472-035-3

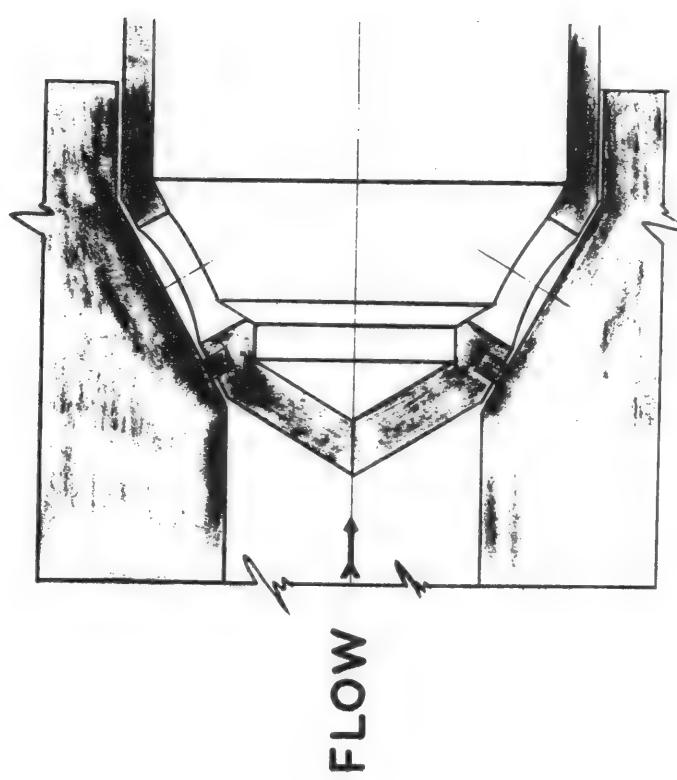
FUEL DUAL-CHECK VALVE



FUEL DUAL CHECK VALVE

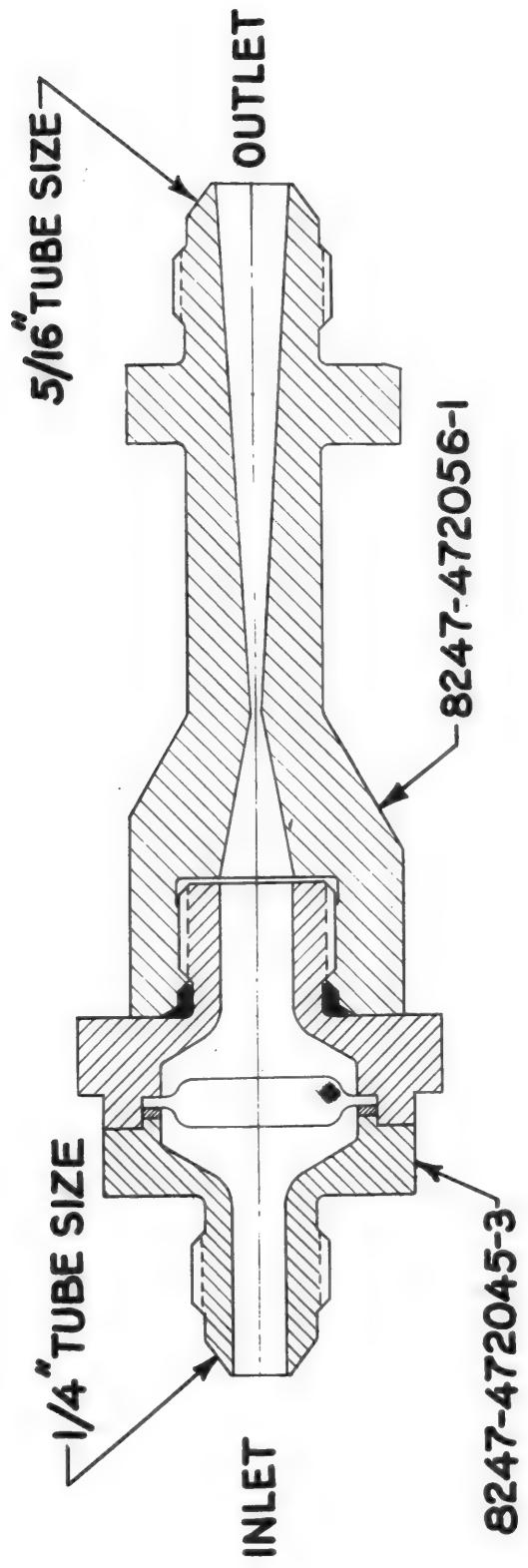


8247-472-040-5



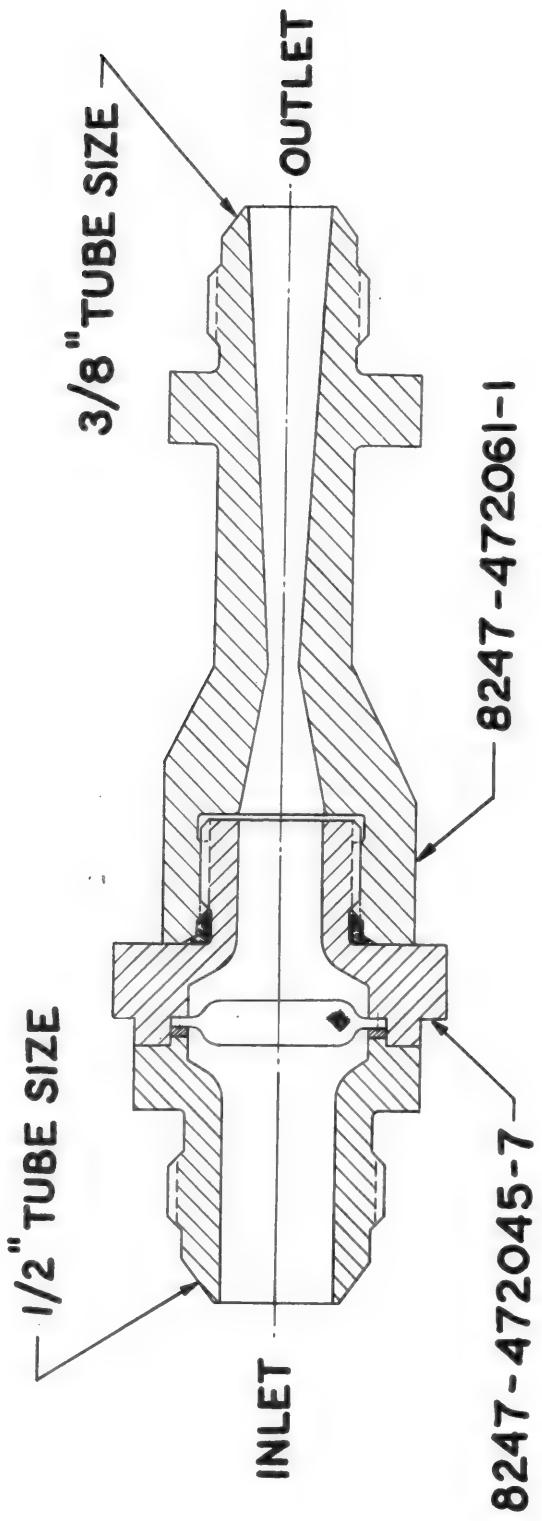
8247-472-040-1

OXIDIZER VENTURI & FILTER ASSEMBLY



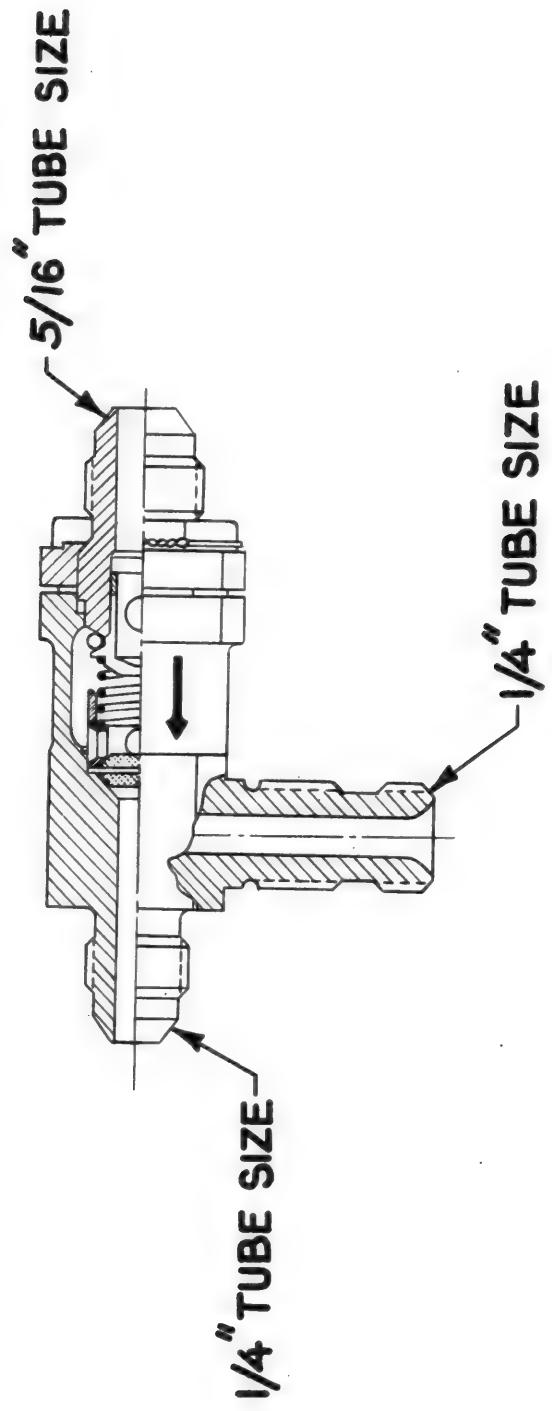
8247-472055-1

FUEL VENTURI & FILTER ASSEMBLY



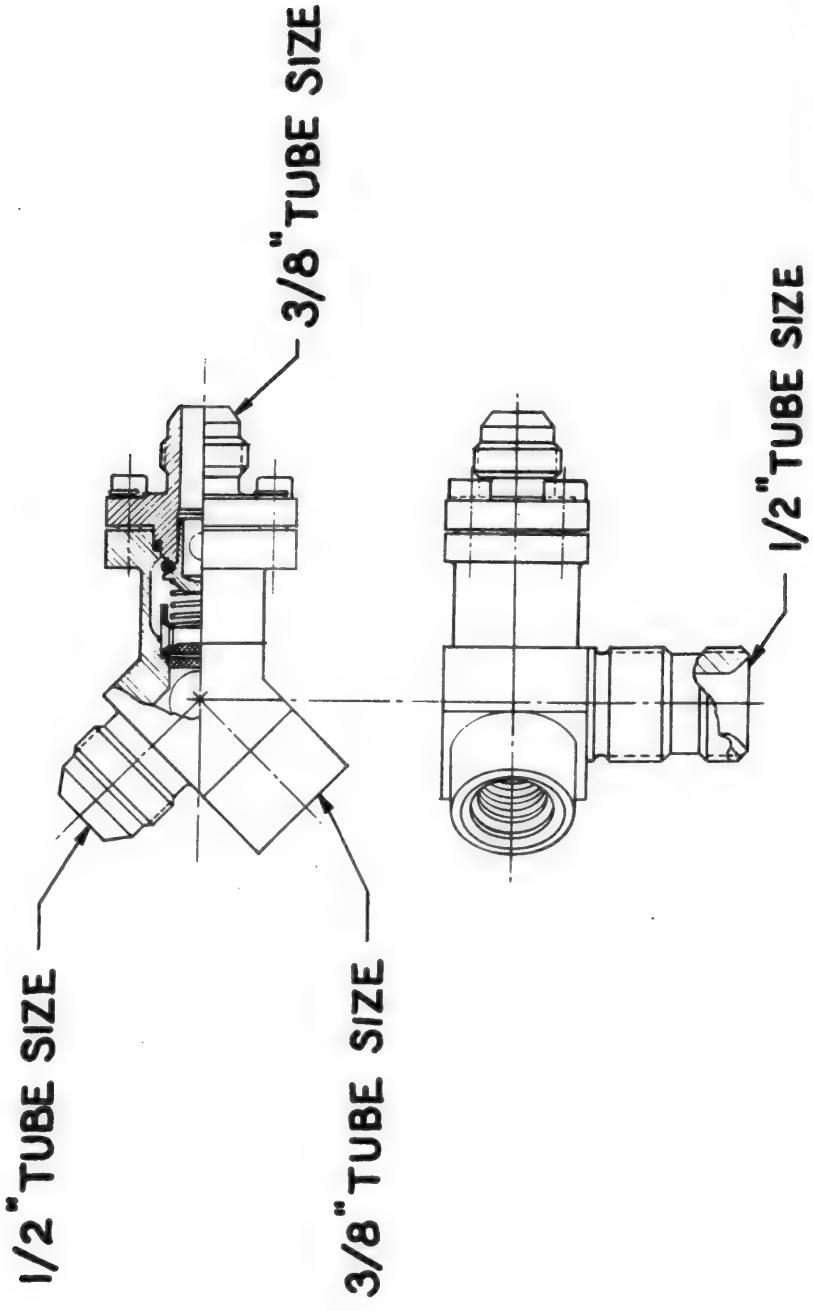
8247-472060-1

OXIDIZER FILL & DRAIN VALVE



8247-472065-1

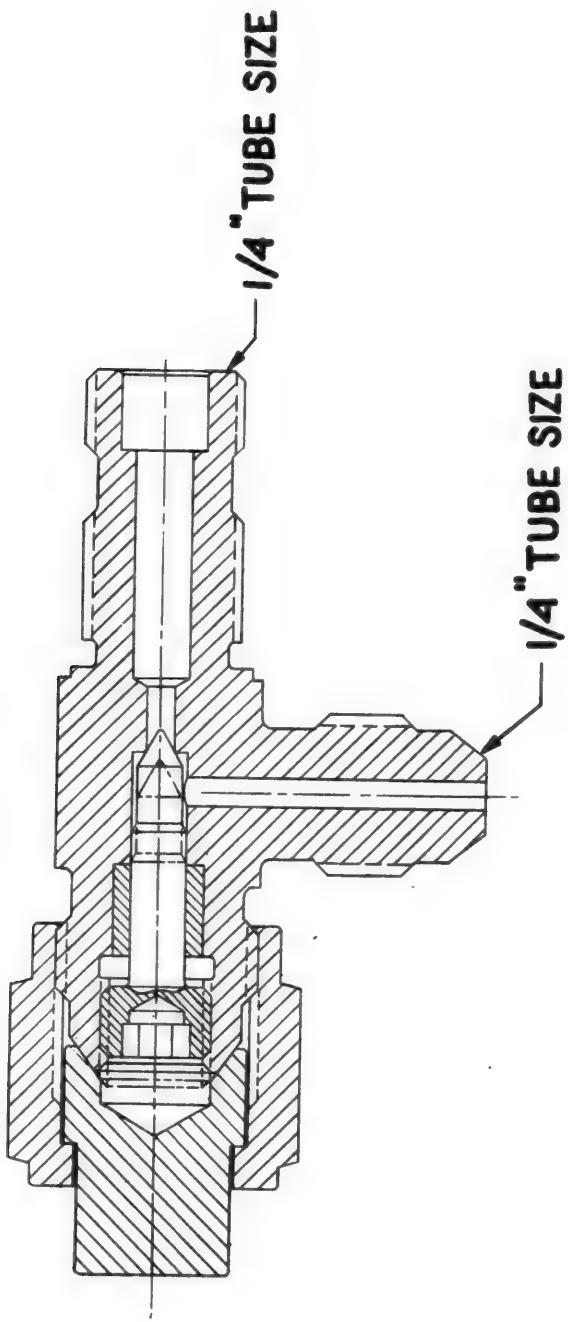
FUEL FILL & DRAIN VALVE



8247-472070-1

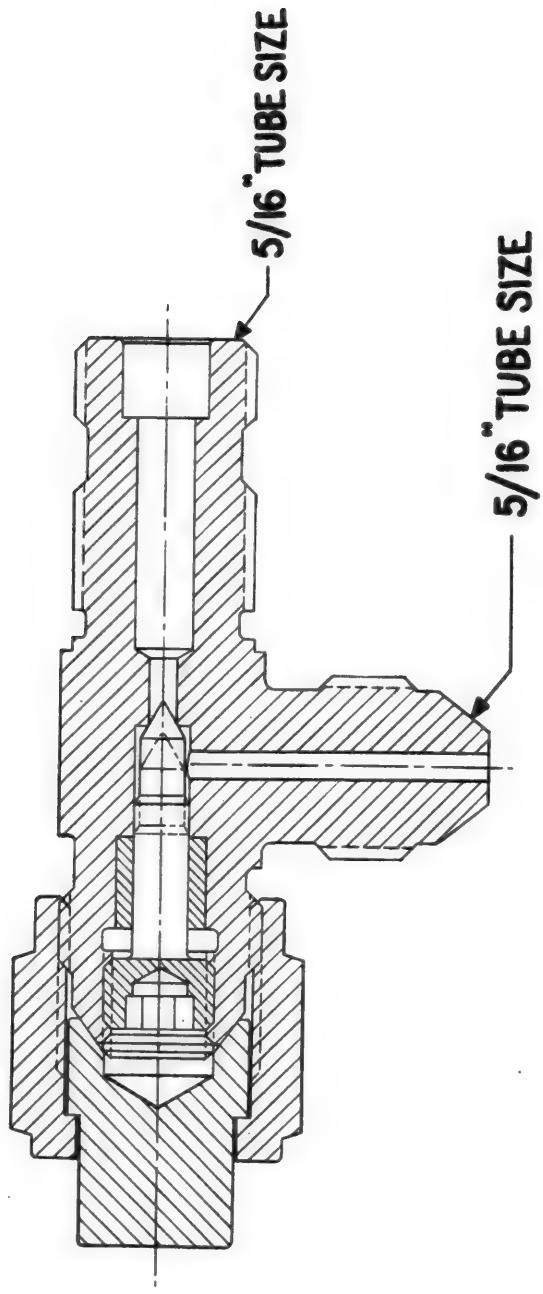
62

OXIDIZER BLEED VALVE



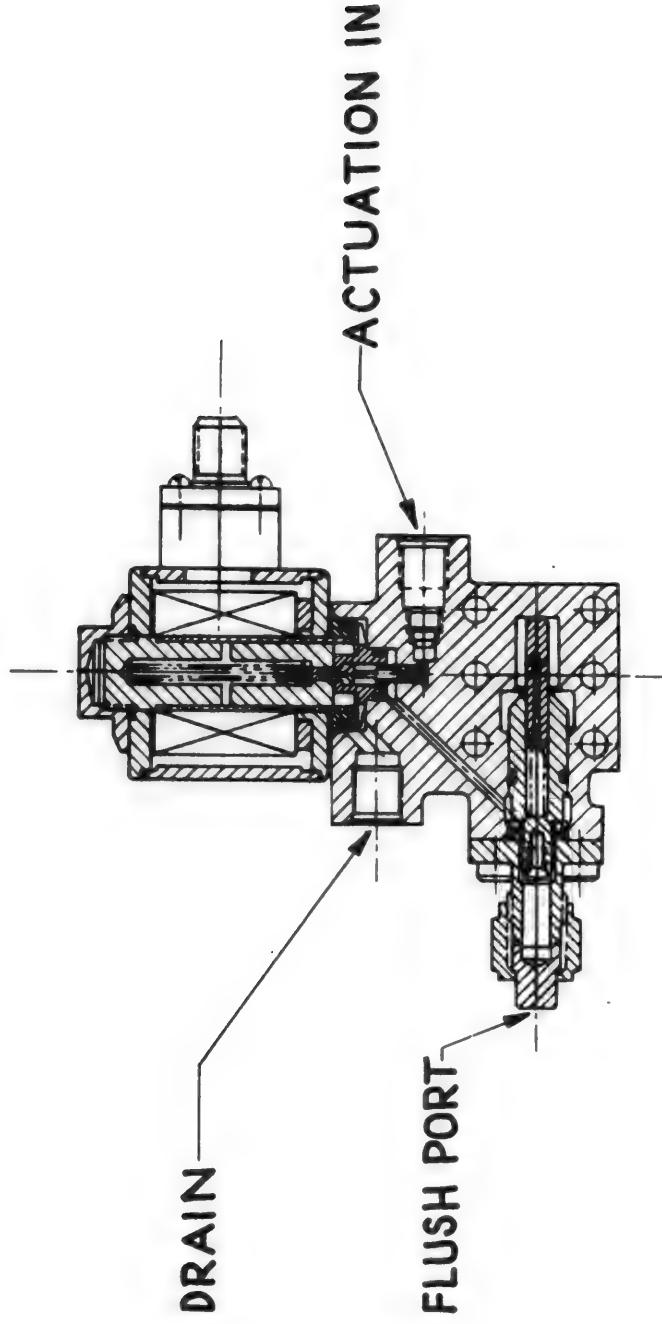
8247-472075-1

FUEL BLEED VALVE



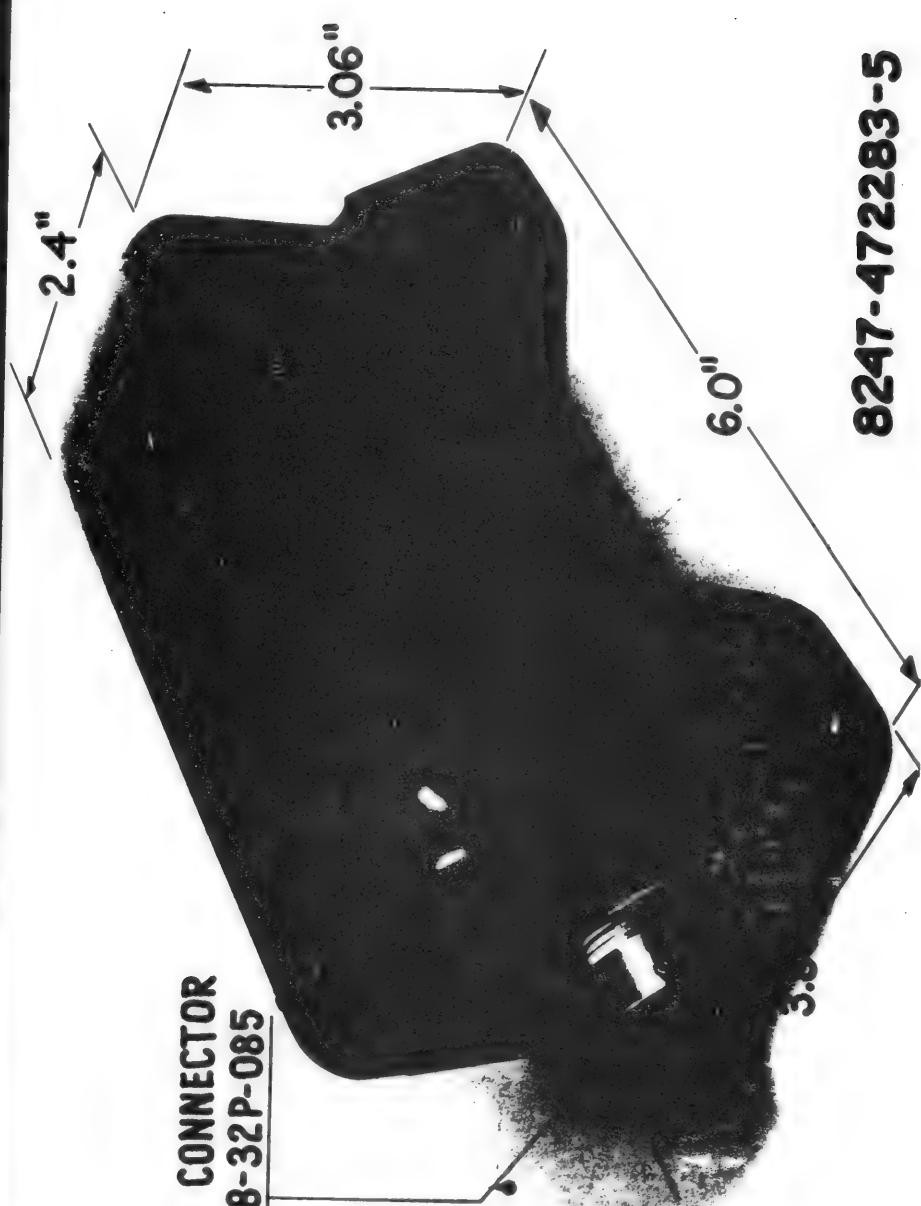
8247-472-080-1

PILOT OPERATED SOLENOID VALVE

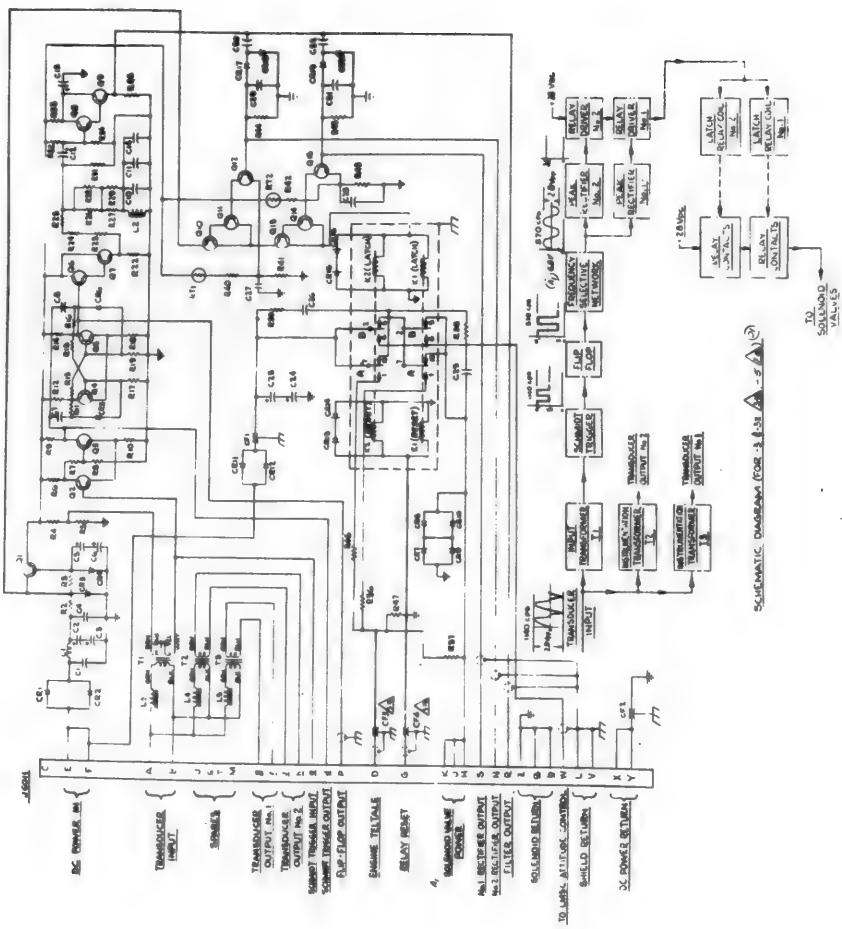


8247-472015-3

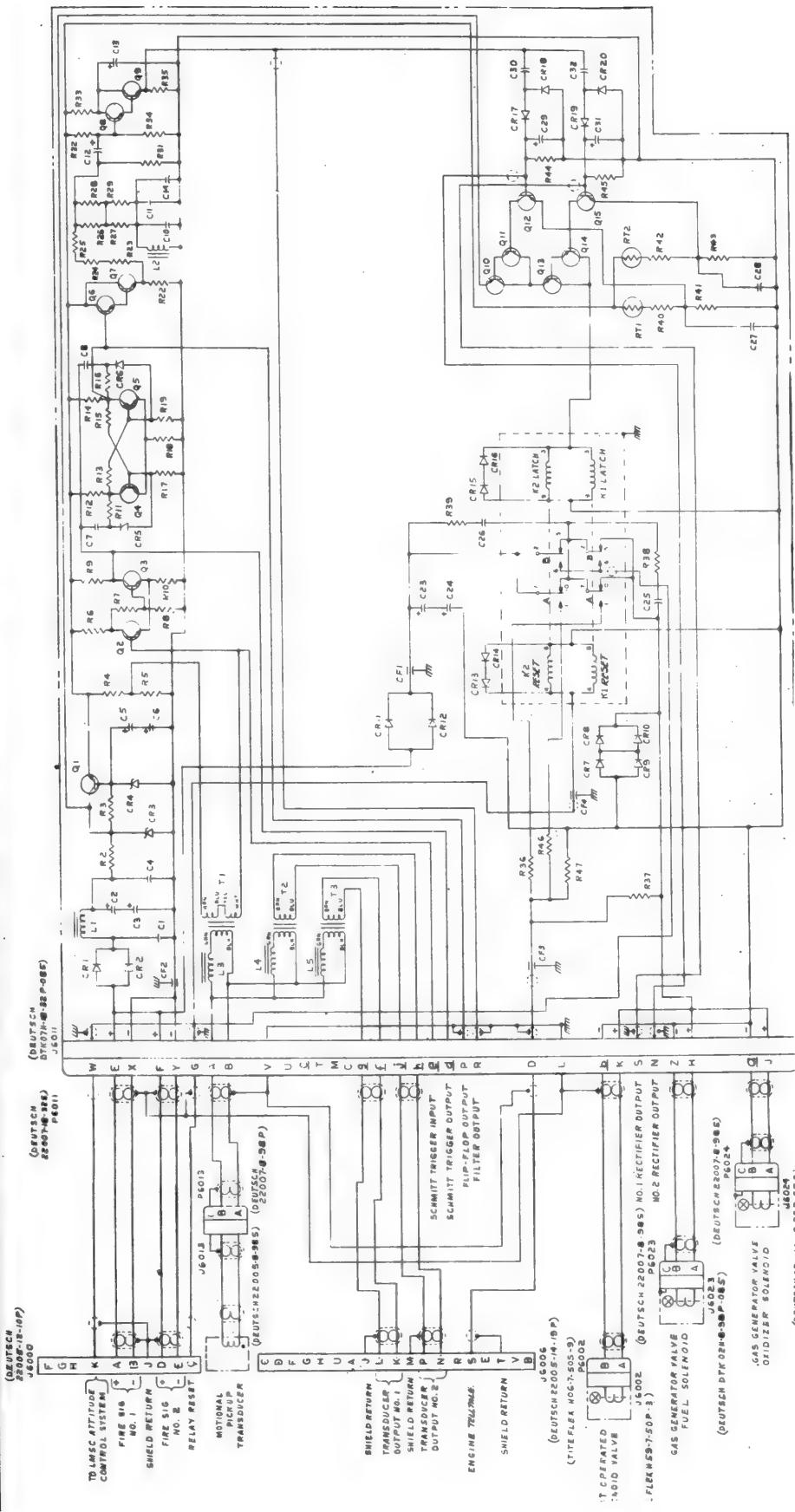
ELECTRONIC GATE ASSEMBLY



SCHMATIC DIA. ELECTRONIC GATE



SCHEMATIC DIA. ELECTRICAL SYSTEM





GEMINI AGENA TARGET VEHICLE

SECONDARY PROPULSION SYSTEM

BAC MODEL 8250

NITROGEN GAS FILTER

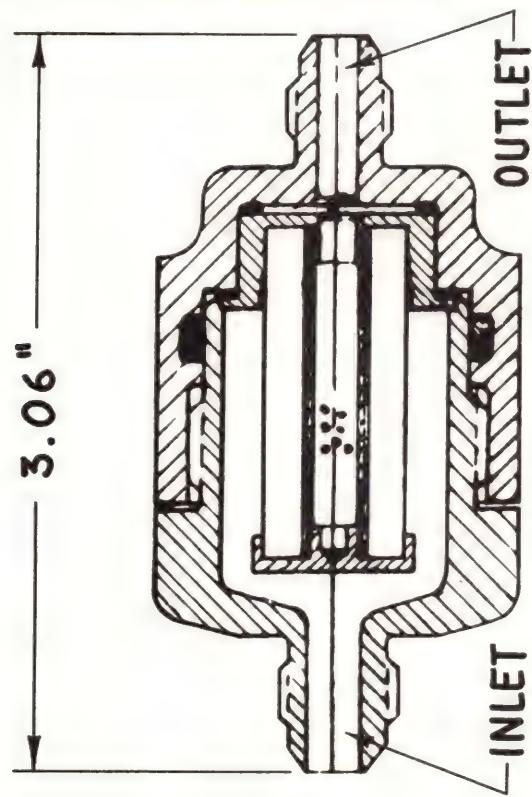
TYPE AND DESCRIPTION	IN-LINE, PLEATED CYLINDRICAL, 5/ ₁₅ MICRON ELEMENT		
PRIMARY FUNCTION	TO PREVENT CONTAMINATION, LARGER THAN 15 MICRON (APPROX. 0.006) FROM ENTERING THE SYSTEM		
PART NUMBER	8101-472155-1		
TYPE OF TESTS	COMPONENT DEVELOPMENT TESTS		
PROBLEMS AND CORRECTIONS	NONE		
QUALIFICATION	COMPONENT PFRT		
FLIGHT HISTORY	NO KNOWN PROBLEMS		
PROBLEMS SINCE QUALIFICATION	TEARDOWN INSPECTION REVEALED AN OPEN GASKE T JACKET, EXPOSING THE ASBESTOS		

NITROGEN GAS FILTER

PART NUMBER	8250-472075-1
TYPE OF CHANGES FROM 8/01	ADDED CLEANLINESS CONTROL ; CHANGED ASBESTOS CORED GASKET TO SOLD ALUMINUM GASKET
TYPE OF TESTS	SYSTEM R&D TEST
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	SYSTEM PFRT
PROBLEMS SINCE QUALIFICATION	NONE

GAS FILTER

PROPELLANT FILTER - UNIT II



8250-472075-1

8250-472010-11

START VALVE

TYPE AND DESCRIPTION

SOLENOID, COAXIAL, NORMALLY CLOSED

PRIMARY FUNCTION

STARTS AND STOPS THE FLOW OF SOURCE GAS PRESSURE

PART NUMBER

8101-472025-1

TYPE OF TESTS

COMPONENT DEVELOPMENT TESTS

PROBLEMS AND CORRECTIONS

NONE

QUALIFICATION

COMPONENT PFR7

FLIGHT HISTORY

NO KNOWN PROBLEMS

PROBLEMS SINCE QUALIFICATION

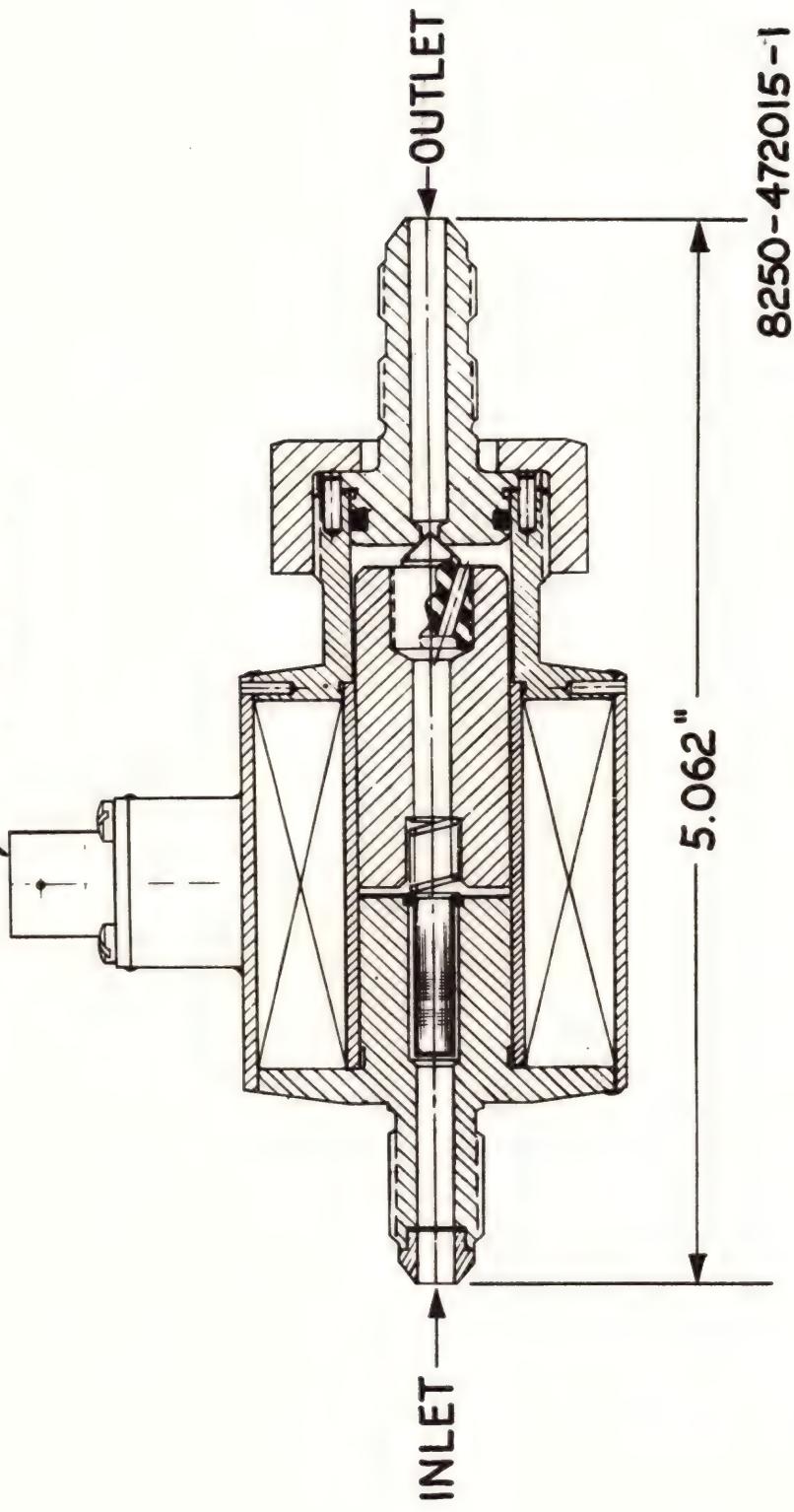
OUTER SURFACE INDICATED SLIGHT RUST
NO CORRECTIVE ACTION TAKEN

START VALVE

PART NUMBER	8250-472015-1
TYPE OF CHANGES <i>FROM 8101</i>	ADDED CLEANLINESS CONTROL ; INCREASED NICKEL PLATING AND CONTROLLED POROSITY
TYPE OF TESTS	SYSTEM R & D TESTS
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATIONS	SYSTEM PFRT
PROBLEMS SINCE QUALIFICATION	START VALVE FROM ONE PVA SYSTEM AT SCTB SHOWED EXCESSIVE EXTERNAL RUST

START VALVE

ELECTRICAL CONNECTOR



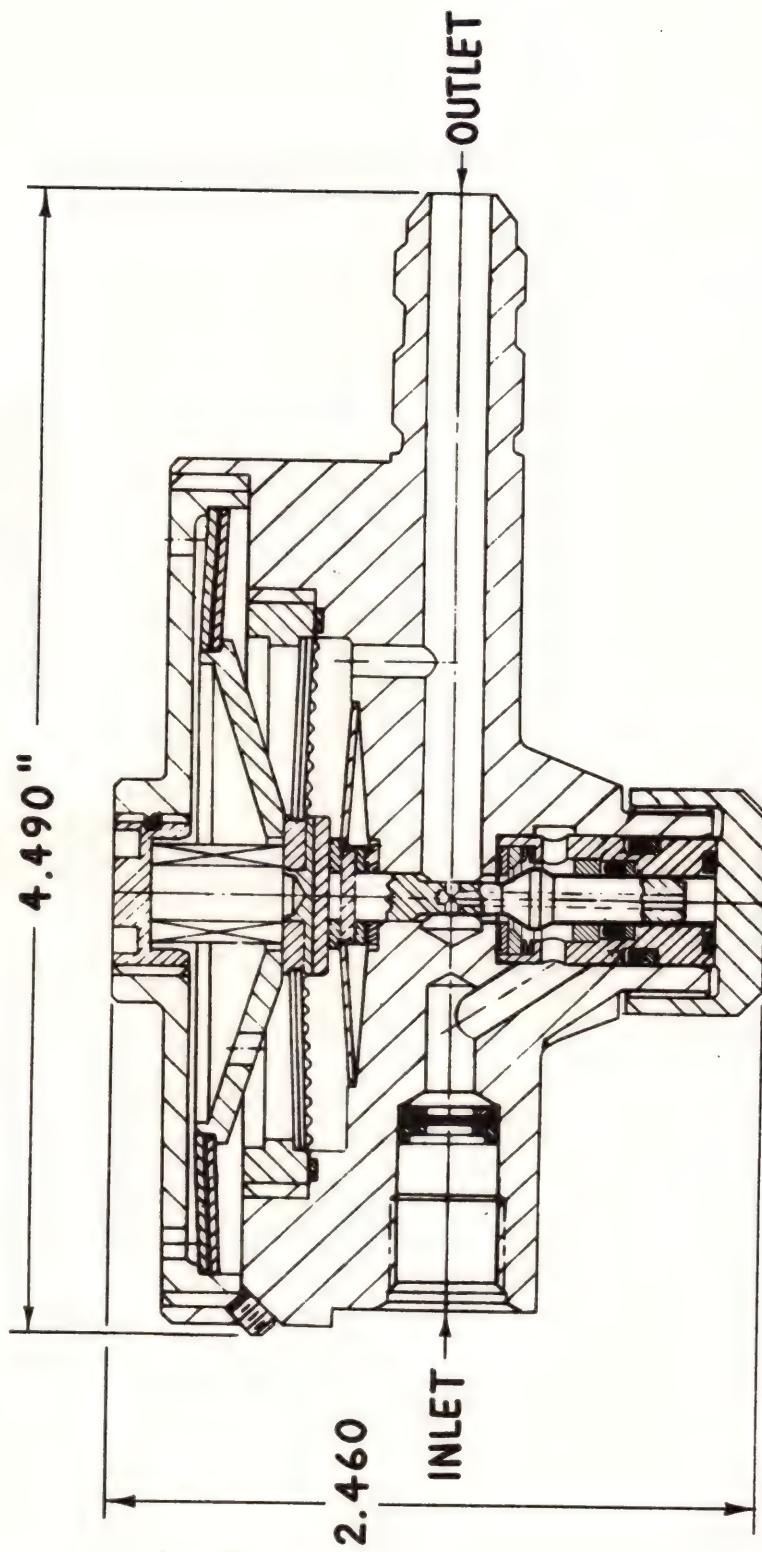
NITROGEN GAS REGULATOR

TYPE AND DESCRIPTION	SINGLE STAGE REGULATOR, SPRING LOADED DOME
PRIMARY FUNCTION	TO CONVERT VARYING SOURCE GAS PRESSURE TO REGULATED PRESSURES
PART NUMBER	8101-472030-1
TYPE OF TESTS	COMPONENT DEVELOPMENT TESTS
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATIONS	COMPONENT PFR7 — THE UNIT FAILED TO MEET HOT TEST REQUIREMENTS
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	NONE

NITROGEN GAS REGULATOR

PART NUMBER	8250-472065-5		
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; SEAT HEAT STABILIZATION; CONTROLLED SEAT TORQUE		
TYPE OF TESTS	a. COMPONENT DYNAMIC TO 8101 LEVELS b. SYSTEM R & D		
PROBLEMS AND CORRECTIONS	a. DOME SPRING ADJUSTING SCREW INADVERTENTLY MOVED; ADDED LOCKING DEVICE b. COLD FLOW OF SEAT ; PROPOSED DESIGN CHANGE		
QUALIFICATION	SYSTEM PFRT		
PROBLEMS SINCE QUALIFICATION	FAILURES ON PVA AT SCTB (1) 1 UNIT FAILED AT LOCK-UP WITH 4000 PSIG INLET (2) 1 UNIT REGULATED SLIGHTLY HIGH OUT OF SPEC AT LOW FLOW ; AUTHORIZED SEAT REDESIGN, 1 UNIT IN INFORMAL QUAL TEST INCLUDING HOT, COLD, DYNAMIC, & 6-MONTH STORAGE TEST		

GAS PRESSURE REGULATOR



8250-472065-1

NITROGEN GAS CHECK VALVE

TYPE AND DESCRIPTION	CIRCLE SEAL RUBBER "O" RING
PRIMARY FUNCTION	USED TO MAINTAIN TANK PRESSURE
PART NUMBER	8101-472080-3
TYPE OF TESTS	COMPONENT DEVELOPMENT TESTS
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATIONS	COMPONENT PFRT
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	NONE

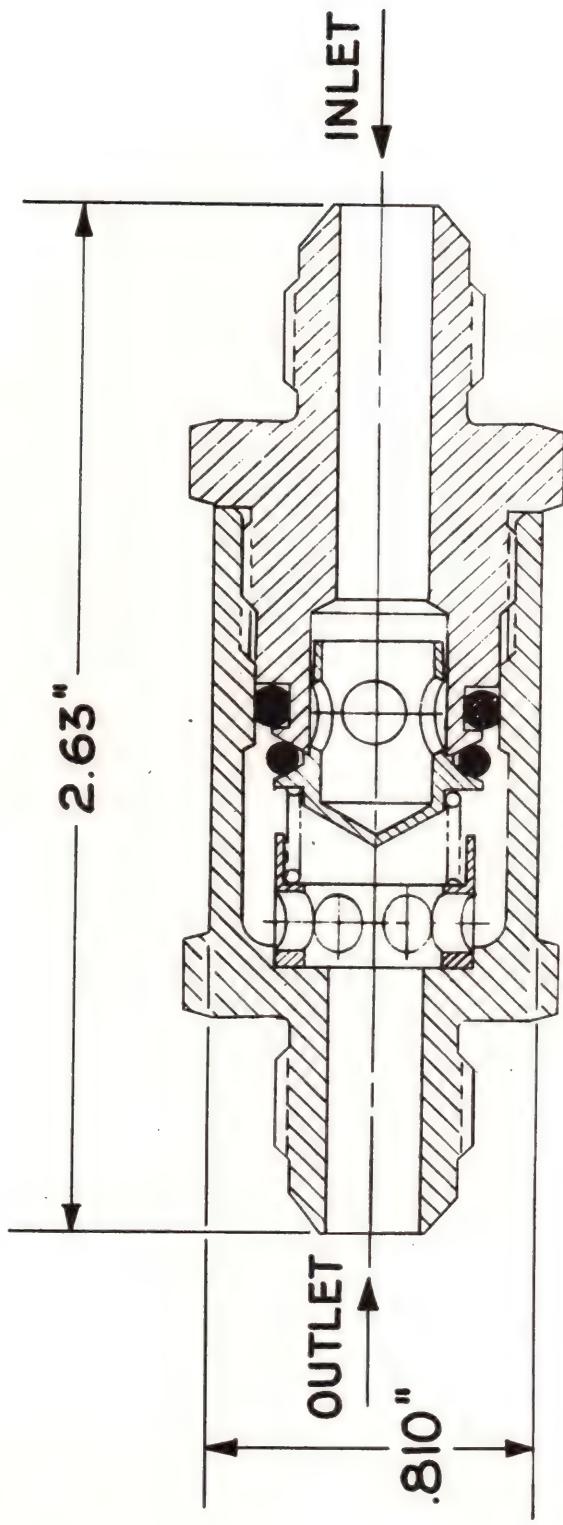
NITROGEN GAS CHECK VALVE

PART NUMBER 8250-472090-1

TYPE OF CHANGES
FROM 8101
ADDED CLEANLINESS CONTROL

TYPE OF TESTS	SYSTEM R & D	SUSPECTED CRACKING PRESSURE PROBLEM; CHANGED PROCEDURES
PROBLEMS AND CORRECTIONS		
QUALIFICATIONS	SYSTEM PFRT	
PROBLEMS SINCE QUALIFICATION	NONE	

GAS CHECK VALVE



8250 - 472090-1

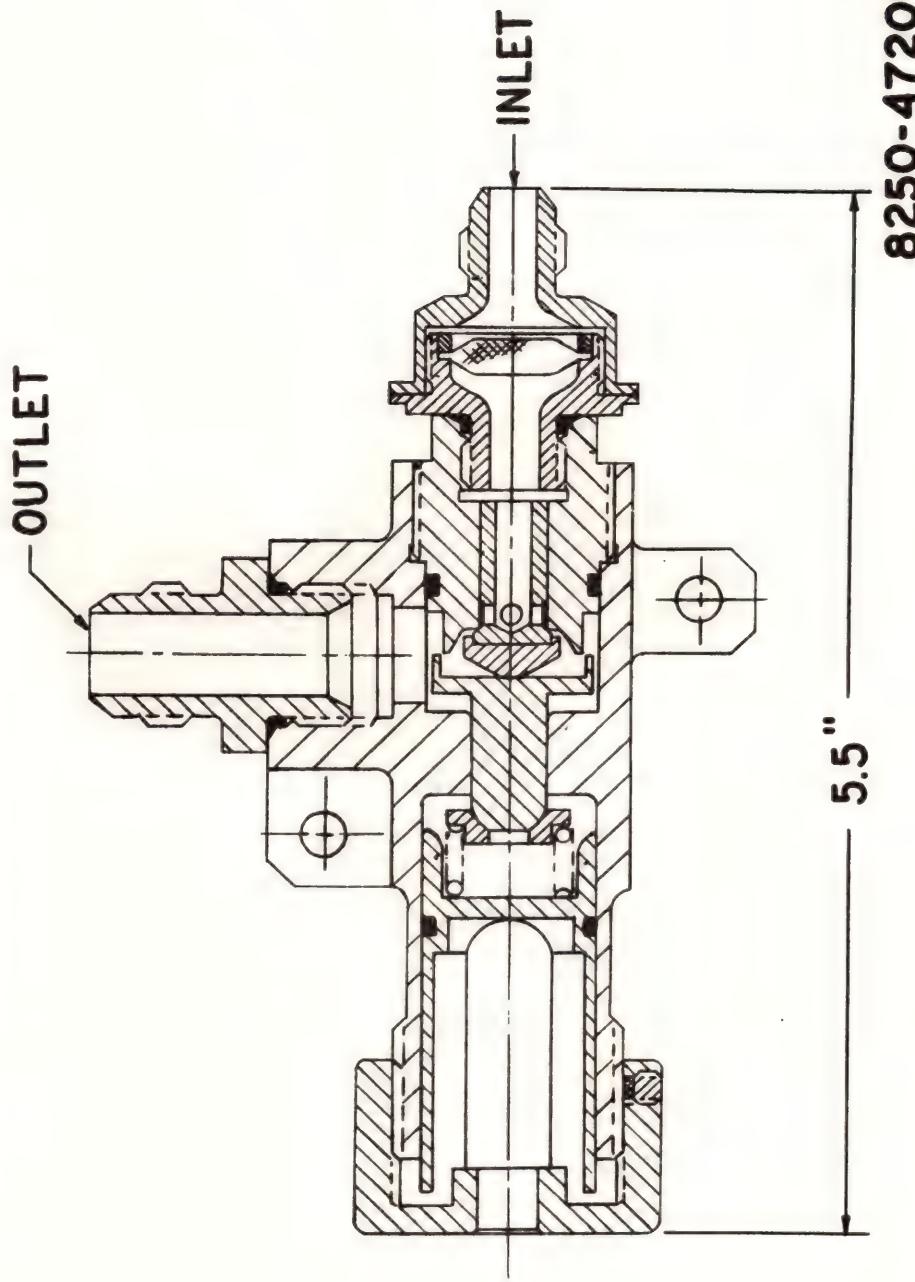
NITROGEN GAS RELIEF VALVE

TYPE AND DESCRIPTION	DIRECT SPRING-LOADED POPPET, EXTERNAL ADJUSTING TYPE
PRIMARY FUNCTION	TO RELIEVE GAS PRESSURE BUILD UP DUE TO THERMAL CONDITIONS AND REGULATOR MALFUNCTION
PART NUMBER	801-472170-3
TYPE OF TESTS	COMPONENT R&D 1000 CYCLES
PROBLEMS AND CORRECTIONS	FAILED DYNAMIC TEST ; SPRING WAS REDESIGNED
QUALIFICATION	COMPONENT PFRT ; LEAKED DURING DYNAMIC TEST
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	NONE

NITROGEN GAS RELIEF VALVE

PART NUMBER	8250-472060-1	TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; CHANGED OUTLET PORT TO $\frac{1}{2}$ TUBE SIZE; DELETED TEST PORT	TYPE OF TESTS	SIMULATED SYSTEM REGULATOR MALFUNCTION SYSTEM R&D	PROBLEMS AND CORRECTIONS	NONE	QUALIFICATION	SYSTEM PFRRT - UNIT WAS READJUSTED	PROBLEMS SINCE QUALIFICATION	ADDED SET SCREW TORQUE AND TORQUE STRIPES REQUIREMENT
-------------	---------------	------------------------------	---	---------------	--	-----------------------------	------	---------------	------------------------------------	---------------------------------	--

GAS PRESSURE RELIEF VALVE



3-WAY VALVE

TYPE AND
DESCRIPTION

SOLENOID ACTUATED, NORMALLY CLOSED

PRIMARY
FUNCTION
TO OPEN AND CLOSE THE PROPELLANT VALVE

PART NUMBER
8101-4722055-5 (UNIT II) 8101-4722055-7 (UNIT I)

TYPE OF TESTS
COMPONENT R&D 10,000 CYCLES

PROBLEMS AND
CORRECTIONS
LEAKAGE DURING VIBRATION

QUALIFICATION
COMPONENT PFRT

FLIGHT HISTORY
NO KNOWN PROBLEMS

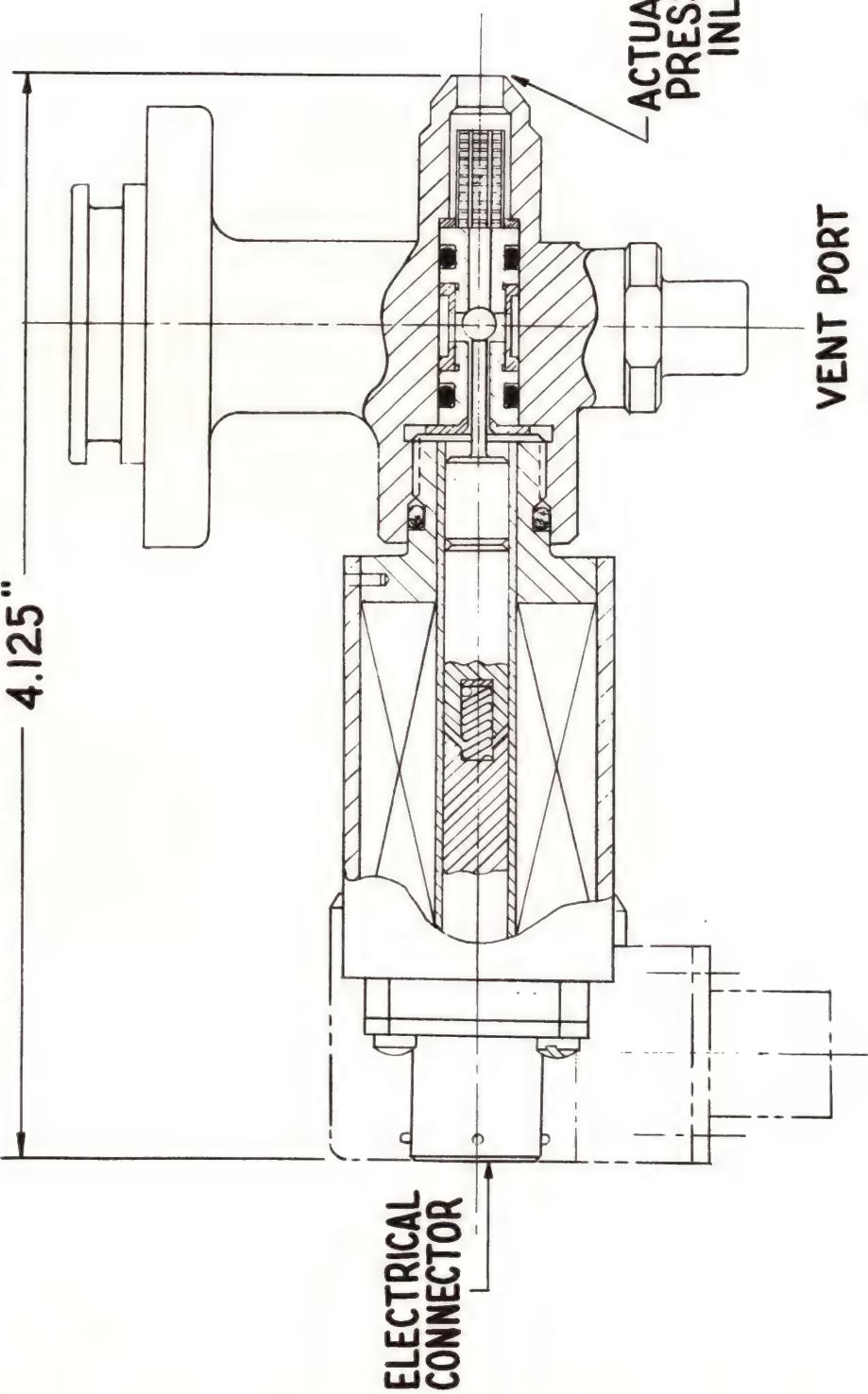
PROBLEMS SINCE
QUALIFICATION
SLIGHT RUST ON OUTER COIL HOUSING

3-WAY VALVE

PART NUMBER	8250-472045-11 (UNIT I) -33 (UNIT II)
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; ADDED FILTER AT VENT PORT; ADDED HEAVIER NICKEL PLATE & CONTROLLED POROSITY
TYPE OF TESTS	R & D DYNAMIC TEST OF VENT FILTER UNIT ONLY TO 8101 LEVELS; SYSTEM R & D (ON TCA)
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	SYSTEM PFRT (ON TCA)
PROBLEMS SINCE QUALIFICATION	EXTERNAL RUST ON PVA UNITS AT LMSC

THREE WAY SOLENOID VALVE

4.125"



8250-472045-1,3

PROPELLANT VALVE INLET FILTERS

TYPE AND
DESCRIPTION
25/40 MICRON "M"SHAPE FILTER ELEMENT

TO FILTER THE PROPELLANTS FROM TANKS

PRIMARY
FUNCTION

PART NUMBERS

UNIT I 8101-472126-1 OXIDIZER
UNIT I 8101-472126-3 FUEL
UNIT II 8101-472125-3 OXIDIZER & FUEL

R&D TESTS ON PROP. VALVE

PROBLEMS AND
CORRECTIONS

NONE

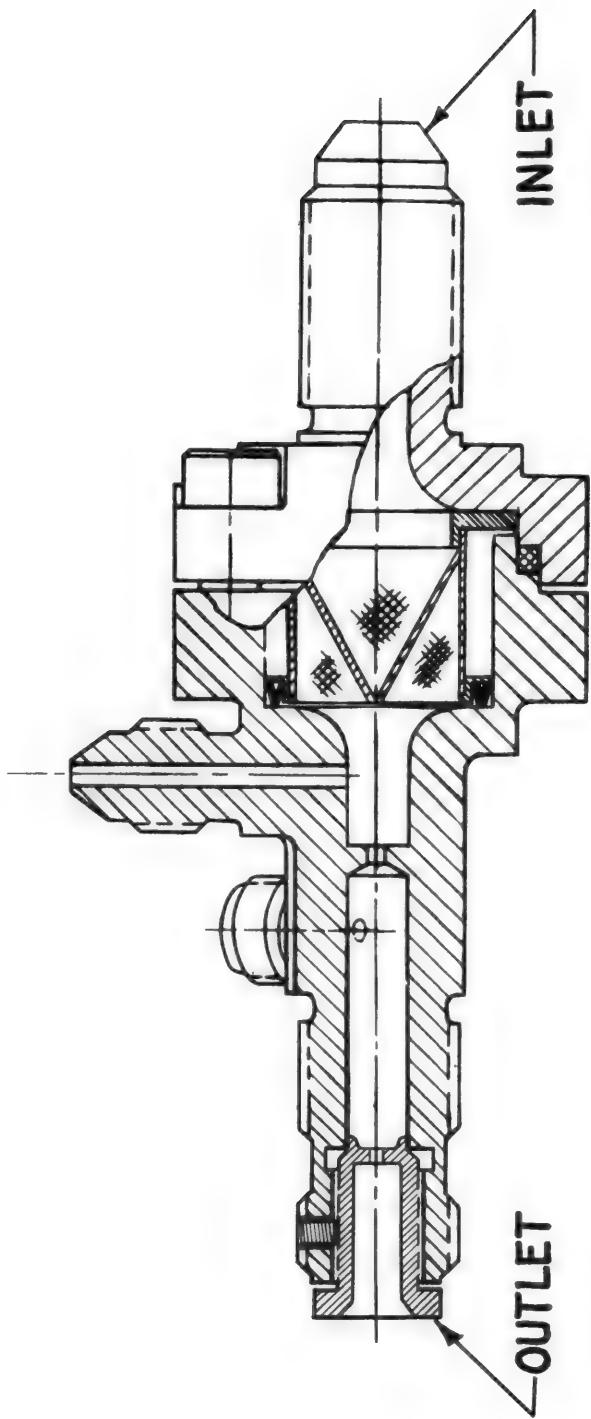
FLIGHT HISTORY
NO KNOWN PROBLEMS

PROBLEMS SINCE
QUALIFICATION

PROPELLANT VALVE INLET FILTER

PART NUMBER	UNIT I	8250-472010-7	OX
	UNIT I	8250-472010 -9	FUEL
	UNIT II	8250-472010-11	OX & FUEL
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; CHANGED 350 MICRON FILTER TO 25/40 AND ADDED SEAL ; UNIT II $\frac{1}{2}$ " T.S INLET PORT WAS $\frac{3}{8}$ " T.S.		
TYPE OF TESTS	SYSTEM R&D		
PROBLEMS AND CORRECTIONS	NONE		
PROBLEMS SINCE QUALIFICATION	CHANGED TRIM ORIFICE CONFIGURATION TO EXPEDITE T.C. A/T		

PROPELLANT FILTER - UNIT I



8250-472010-749

PROPELLANT VALVES

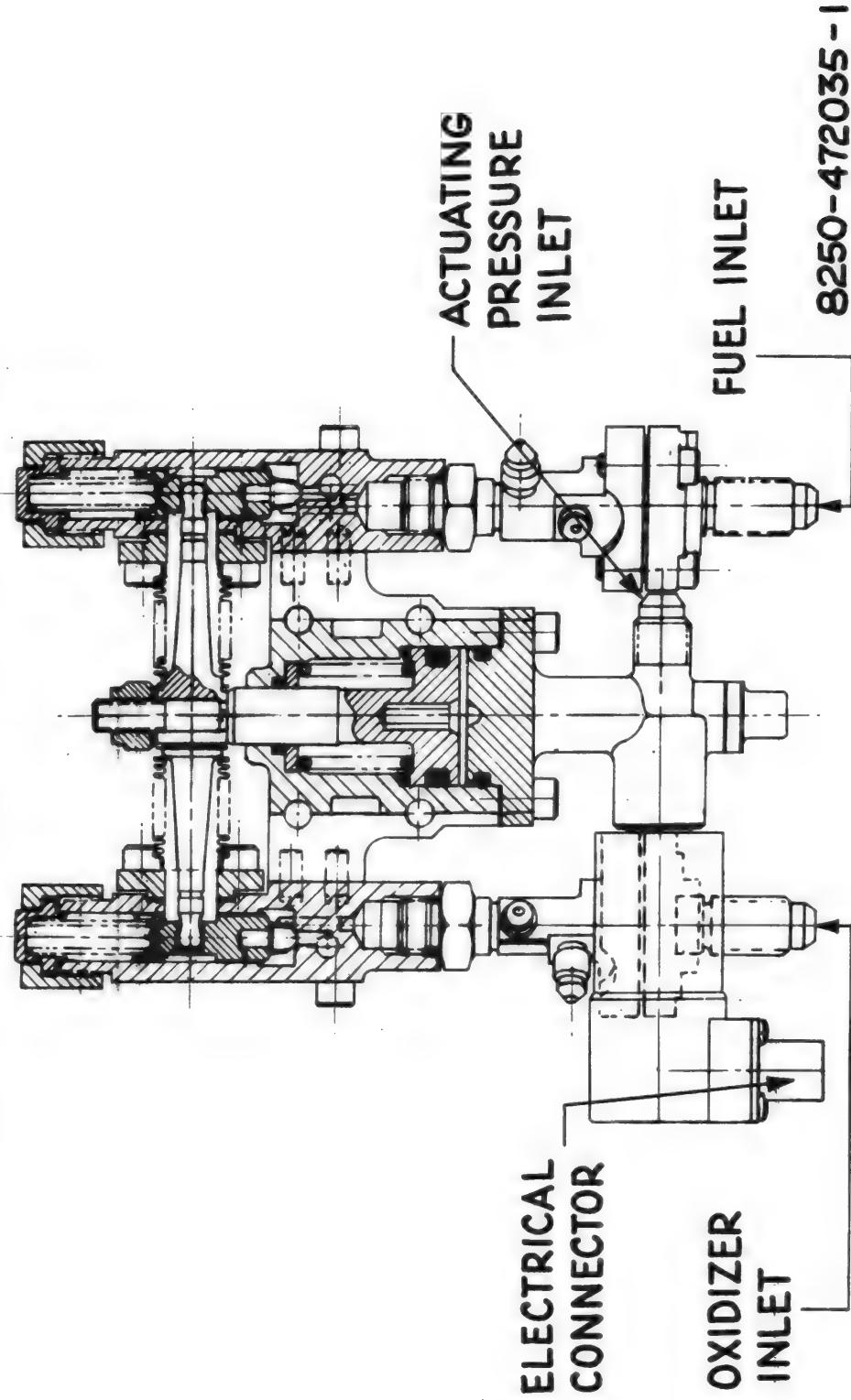
TYPE AND DESCRIPTION	YOKÉ TYPE, GAS ACTUATED
PRIMARY FUNCTION	TO START & STOP THE FLOW OF PROPELLANTS
PART NUMBERS	UNIT I 8101-472095-9 ; UNIT II 8101-472100-7
TYPE OF TEST	COMPONENT R&D 1000 CYCLES EACH
PROBLEMS AND CORRECTIONS	DEFORMATION OF THE KEL-F TIP ; IMPOSED LIMITATION ON UNIT II ONLY
QUALIFICATION	AT THRUST CHAMBER LEVEL ; NOTED SALTS ON OX SIDE
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	YOKÉ BELOW FAILURE ; PITTING CORROSION ; IMPOSED RIGID FABRICATING CONTROLS ON VENDOR

PROPELLANT VALVES

PART NUMBERS	UNIT I 8250-472035-5	UNIT II 8250-472040-5
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL ; FILTERED VENT AT ACTUATING CHAMBER	
TYPE OF TESTS	SYSTEM R&D	
PROBLEMS AND CORRECTIONS	ADDITION OF VENT FILTERS REQUIRED INCREASE IN RESIDUAL IMPULSE	
QUALIFICATION	SYSTEM PERT ; SALTS ON OXIDIZER SIDE CHANGED ALUMINUM GASKETS TO GOLD	
PROBLEMS SINCE QUALIFICATION	NONE — UNIT I, ADDED BACK-UP RING AND CHANGED NUT TO LIQUID FILTER INLET CONNECTION	

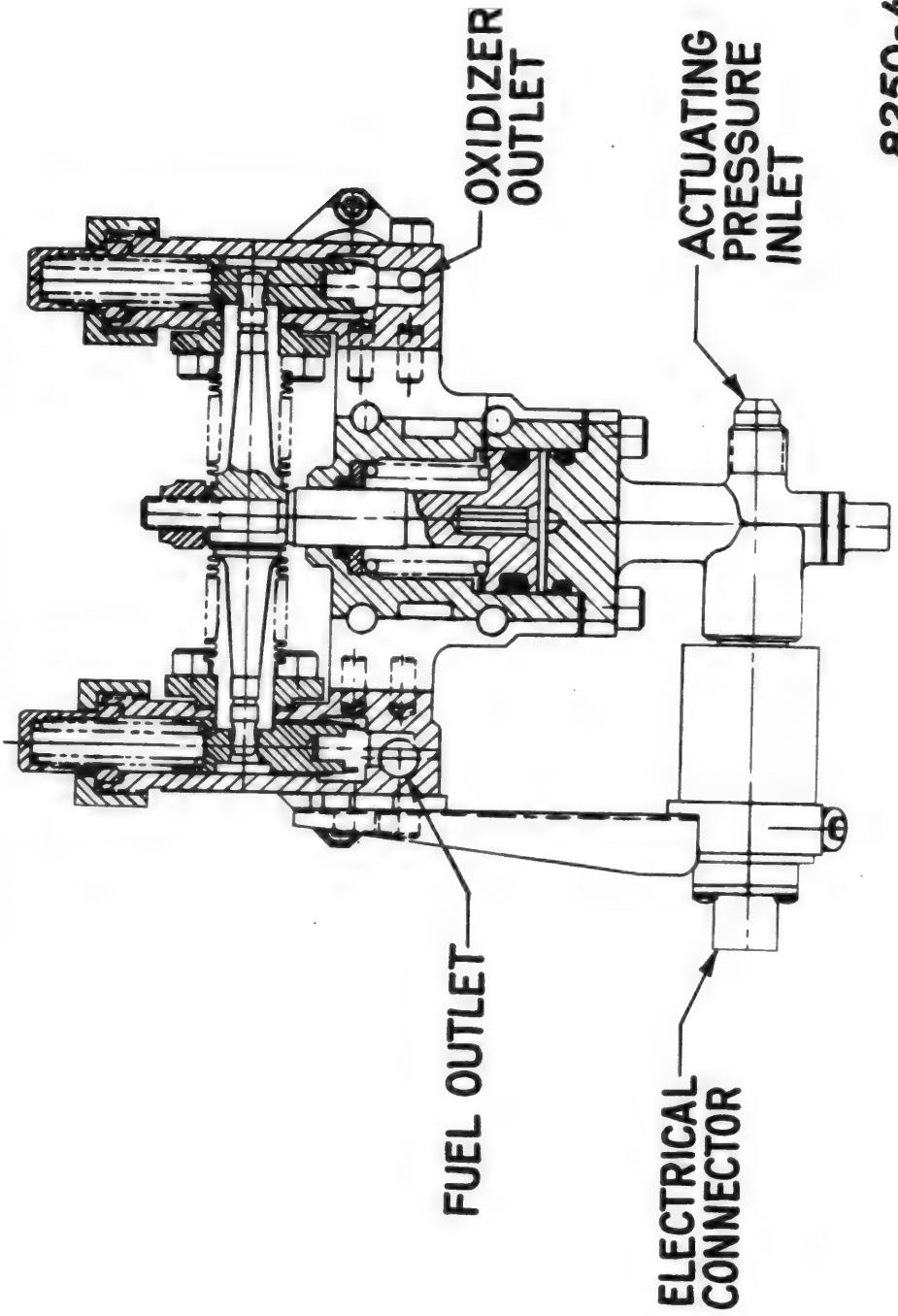
2

PROPELLANT VALVE - UNIT I



93

PROPELLANT VALVE - UNIT II



8250-472040-1

94

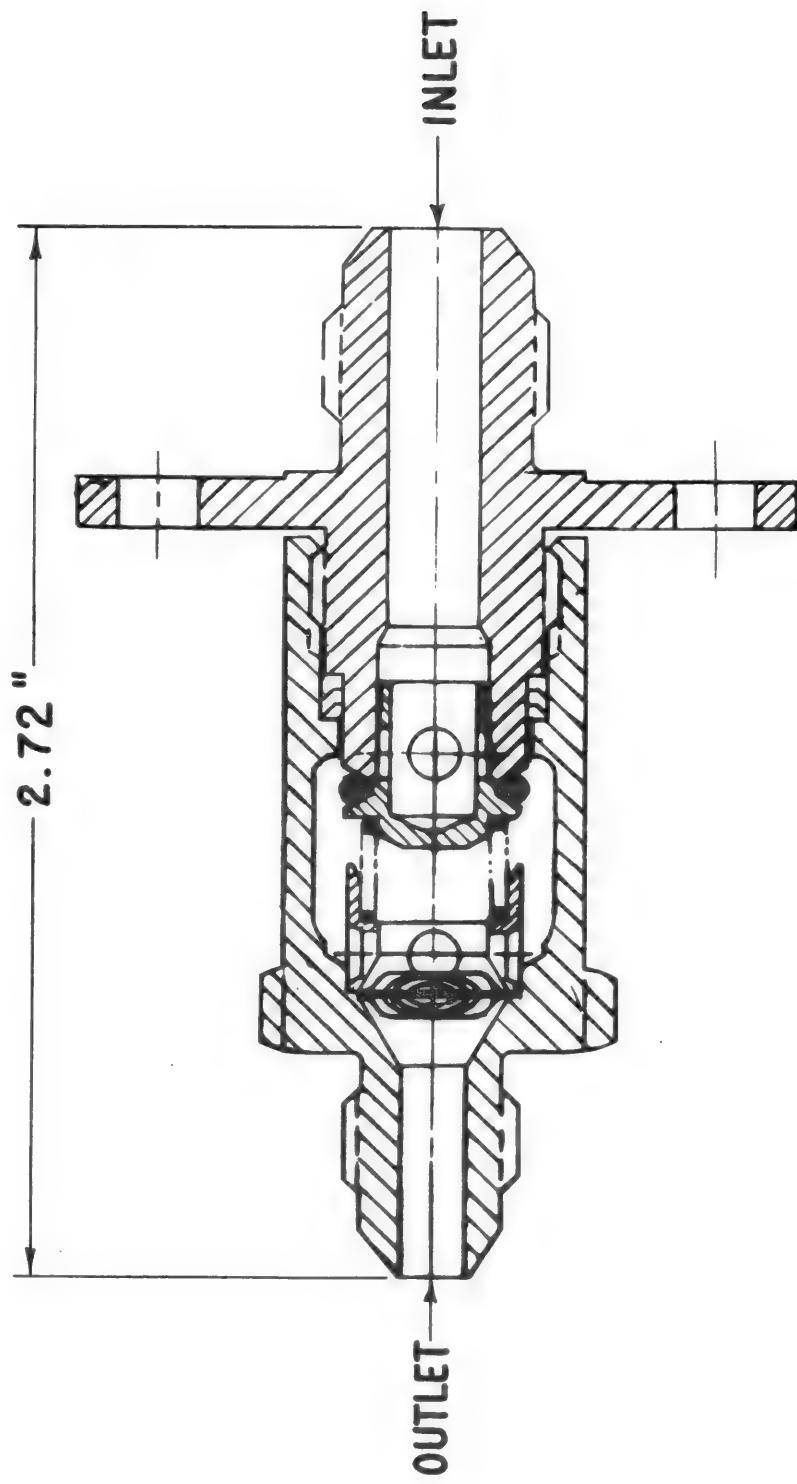
OXIDIZER FILL AND DRAIN VALVE

TYPE AND DESCRIPTION	CHECK VALVE WITH MOUNTING LUGS
PRIMARY FUNCTION	TO FILL AND DRAIN THE MON SYSTEM
PART NUMBER	8101-472045-1
TYPE OF TESTS	COMPONENT R & D 1000 CYCLES
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	COMPONENT PFR7
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	SALTING AND PITTING OF THE ALUMINUM SEALING SURFACES

OXIDIZER FILL AND DRAIN VALVE

PART NUMBER	8250-472001-3
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; CONTROLLED STROKE; FILTER:- CHANGED TO STAINLESS STEEL UNIT AND INLET PORT TO $\frac{3}{8}$ " T. S.
TYPE OF TESTS	COMPONENT R&D DYNAMIC TO 8101 LEVELS SYSTEM R&D
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	SYSTEM PFRT
PROBLEMS SINCE QUALIFICATION	NONE

OXIDIZER FILL VALVE



8250-472001-3

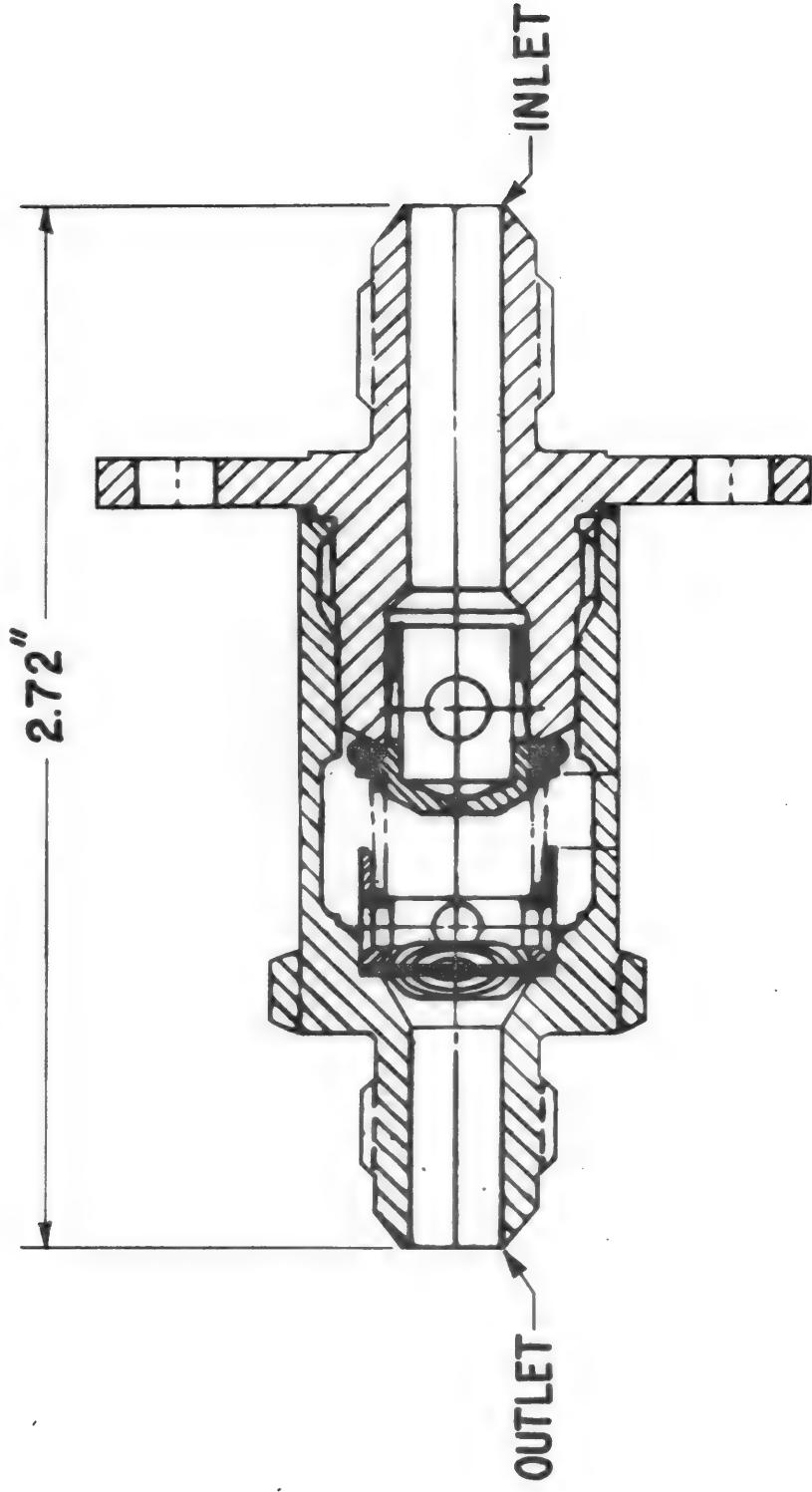
FUEL FILL AND DRAIN

TYPE AND DESCRIPTION	CHECK VALVE WITH MOUNTING LUGS
PRIMARY FUNCTION	TO FILL AND DRAIN UDMH SYSTEM
PART NUMBER	8101-472050-3
TYPE OF TESTS	COMPONENT R&D (-1 TEFLOON O'RING) 1000 CYCLES
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	COMPONENT PFR7 (-1 TEFLOON O'RING)
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	FAILED GAS LEAK CHECK; CHANGED TEFLOON O'RING TO BUTYL RUBBER

FUEL FILL AND DRAIN VALVE

PART NUMBER	8250 - 472005-5
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; CONTROLLED STROKE; FILTER
TYPE OF TESTS	COMPONENT R&D DYNAMIC TO 8101 LEVELS SYSTEM R&D
PROBLEMS AND CORRECTIONS	VALVE HANG-UP; EVALUATED OTHER RUBBER COMPOUNDS
QUALIFICATION	SYSTEM PFR7 WITH MODIFIED ALUMINUM VALVE
PROBLEMS SINCE QUALIFICATION	CHANGED TO ALL STAINLESS VALVE WITH "O"RING SAME AS OX VALVE. CONSIDERED QUALIFIED BY SIMILARITY

FUEL FILL VALVE



8250-472005-3

NITROGEN GAS FILL AND VENT VALVE

TYPE AND DESCRIPTION CHECK VALVE, SIMILAR TO AN815-4 UNION, EXCEPT HAS MOUNTING FLANGES. ALL STAINLESS STEEL; NYLON SEAL USED TO PRESSURIZE AND VENT THE SOURCE BOTTLE IN CONJUNCTION WITH A MANUALLY OPERATED, POPPET UNSEATING TOOL, FROM THE GROUND SERVICE CONSOLE. CAPPED WITH REDUNDANT SEAL FOR FLIGHT.

PRIMARY FUNCTION

PART NUMBER

8101-472020-3

TYPE OF TESTS
PROBLEMS AND CORRECTION

COMPONENT DEVELOPMENT TESTS ON -1
RUBBER O'RING DISLODGED FROM POPPET ON VENT CYCLE (-1 VALVE). CHANGED TO NYLON SEAL AND CONTROLLED POPPET STROKE (-3 VALVE)

QUALIFICATION

COMPONENT PFRT (-1). PENALTY PFRT ON -3
20 HIGH PRESSURE FILL AND VENT CYCLES

FLIGHT HISTORY

NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION NONE

NITROGEN GAS FILL AND VENT VALVE

PART NUMBER 8250-472070-1

TYPE OF CHANGES ADDED CLEANLINESS CONTROL
FROM 8101

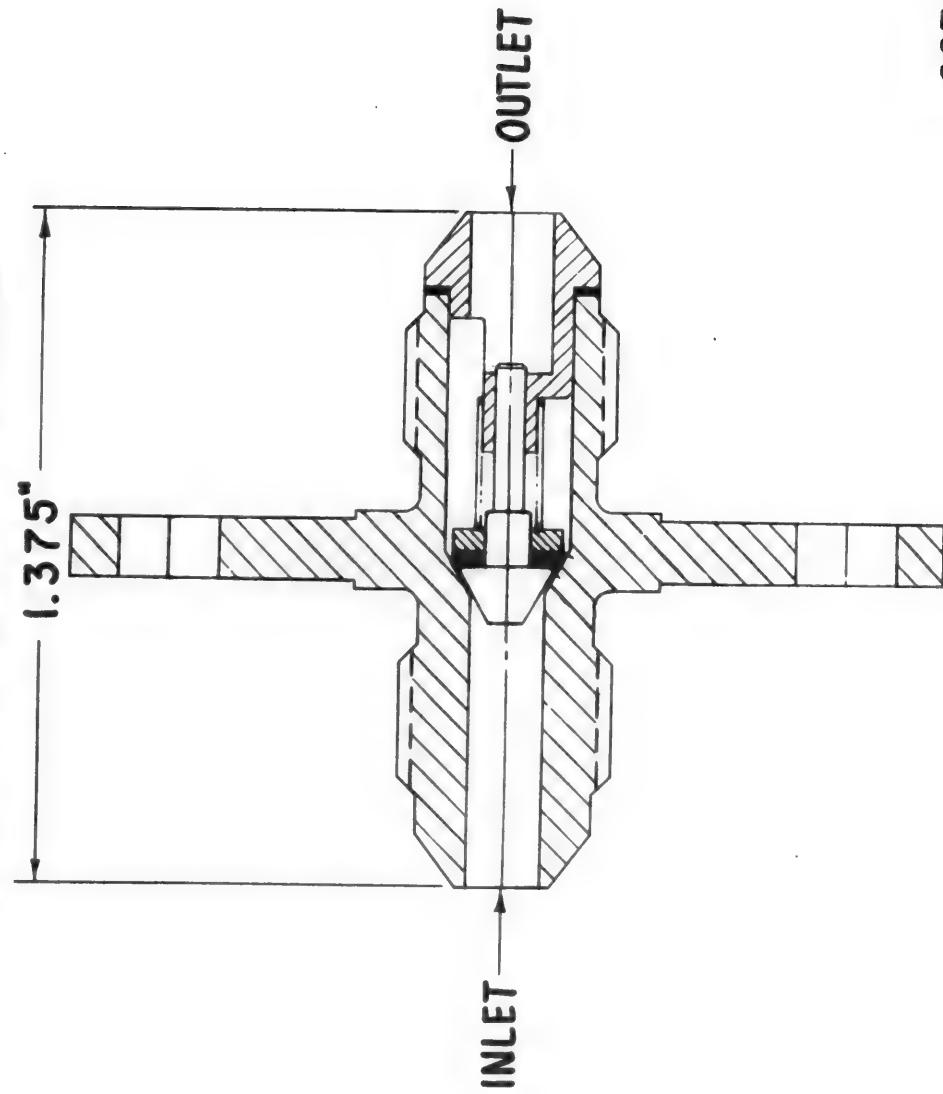
TYPE OF TESTS SYSTEM R&D TESTS

PROBLEMS AND VALVE WAS INSTALLED IN REVERSE : ADDED NOTCH CORRECTIONS ON FLANGE TO MATE WITH PIN ON SERVICE PANEL.
EXPERIENCED VALVE HANG-UP : VENDOR QUALITY INSTRUCTED TO INSPECT FOR NYLON SHREADS, METAL CHIPS, BURRS, AND FINISHES WHICH COULD CAUSE HANG-UP AND LEAKS

QUALIFICATION SYSTEM PFRT

PROBLEMS SINCE NONE
QUALIFICATION

GAS FILL VALVE



8250-472070-1

MANUAL GAS VALVE

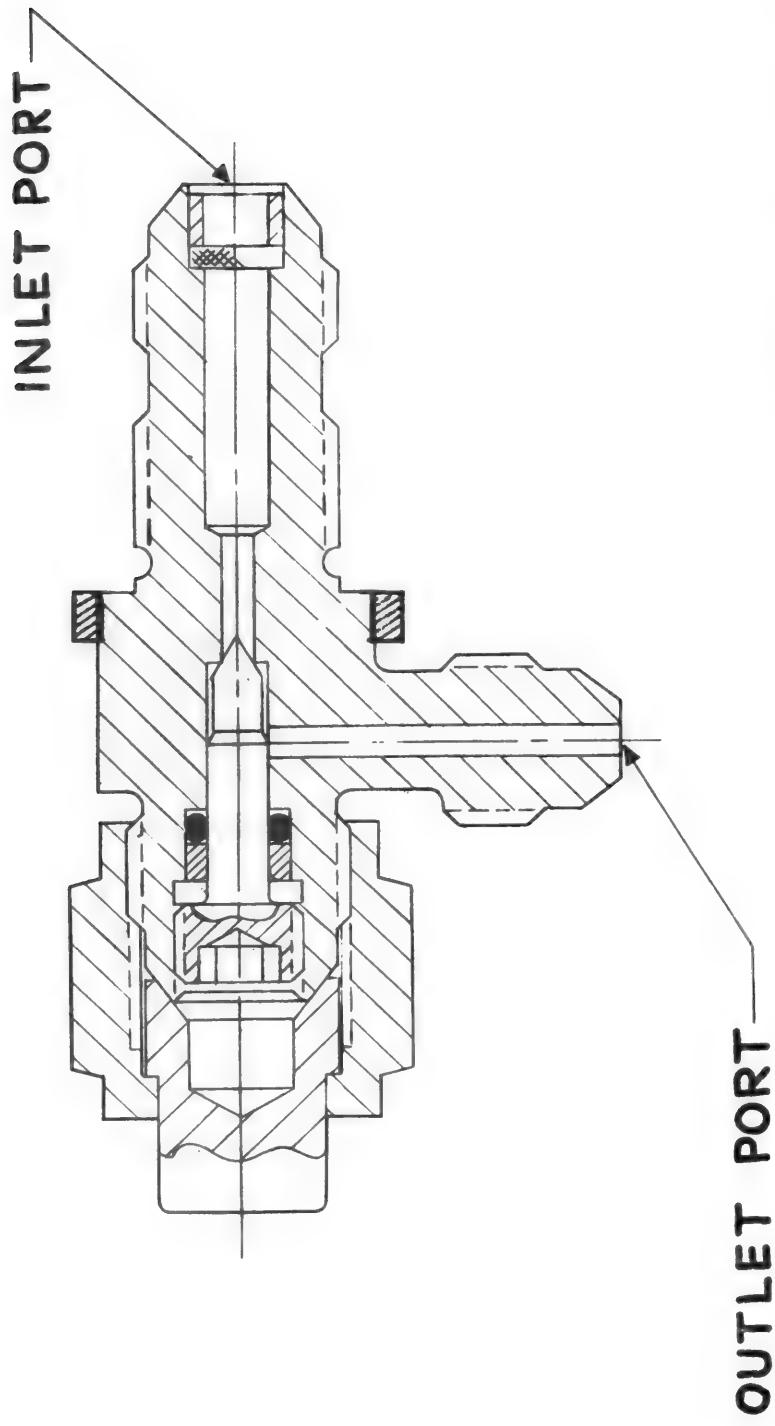
TYPE AND DESCRIPTION	STAINLESS STEEL, METAL TO METAL NEEDLE VALVE SEAT
PRIMARY FUNCTION	USED TO MAINTAIN POSITIVE PRESSURE ON PROPELLANT TANK IN CONJUNCTION WITH GSE CONSOLE
PART NUMBER	8101-472075-1
TYPE OF TESTS	COMPONENT R & D 1000 CYCLES ENDURANCE
PROBLEMS AND CORRECTIONS	NONE
QUALIFICATION	COMPONENT PFR
FLIGHT HISTORY	NO KNOWN PROBLEMS
PROBLEMS SINCE QUALIFICATION	NONE

MANUAL GAS VALVE

PART NUMBER	8250-472050-5			
TYPE OF CHANGES FROM 8101	ADDED CLEANLINESS CONTROL; FILTER ON SYSTEM SIDE OF SEAT; REDUNDANT CAP. CHANGED TEFLON STEM SEAL TO BUTYL RUBBER; GSE ATTACHING PORT FROM $\frac{5}{16}$ TO $\frac{1}{4}$ T.S.			
TYPE OF TESTS	COMPONENT DYNAMIC TO 8101 LEVELS; REDUNDANT STEM SEAL OVER-TORQUE TESTS; R&D SYSTEM			
PROBLEMS AND CORRECTIONS	VALVE MOUNTING PROBLEM; REQUIRED ADDITION OF MOUNTING LUGS; SYSTEM PFRT			
QUALIFICATION	SYSTEM PFRT			
PROBLEMS SINCE QUALIFICATION	NONE			

- O ✓

MANUAL BLEED VALVE



8250 - 472050-5

TANK ISOLATION VALVE

**TYPE AND
DESCRIPTION**

PRIMARY FUNCTION TO ISOLATE THE PROPELLANT TANKS

PART NUMBER 8250-472095-1

TYPE OF TESTS COMPONENT R&D TO 8101 LEVELS, CONDUCTED
1000 ENDURANCE CYCLES, SYSTEM R&D TEST

**PROBLEMS AND
CORRECTIONS**

QUALIFICATION COMPONENT PFRT ; DYNAMIC TESTS TO
8250 COMPONENT LEVELS, SYSTEM PFRT

**PROBLEMS SINCE
QUALIFICATION** NONE

8250 COMPONENT PFRT TESTS FOR ISOLATION VALVE

1. PRESSURES

OPERATING : 205 PSIG

PROOF : 383 PSIG

2. TEST MEDIA : NITROGEN GAS PER MIL-P-2740 (USAF)

3. TEMPERATURE TESTS

a. HIGH TEMP: SOAK AT +160°F FOR 24 HRS, THEN F/T @ +100°F

b. LOW TEMP: SOAK AT -65°F FOR 24 HRS, THEN F/T @ 0°F

4. ENDURANCE TEST

CONDUCT 1000 OPERATING CYCLES

5. FUNCTIONAL TEST

a. LEAKAGE

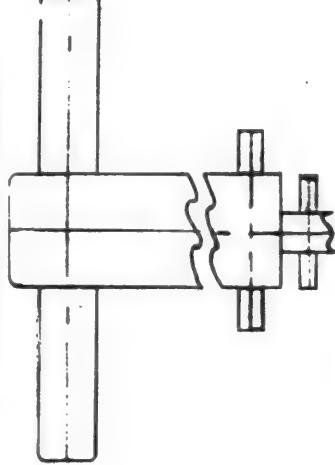
b. FLOW VS PRESSURE DROP

c. ACTUATING TORQUE TEST

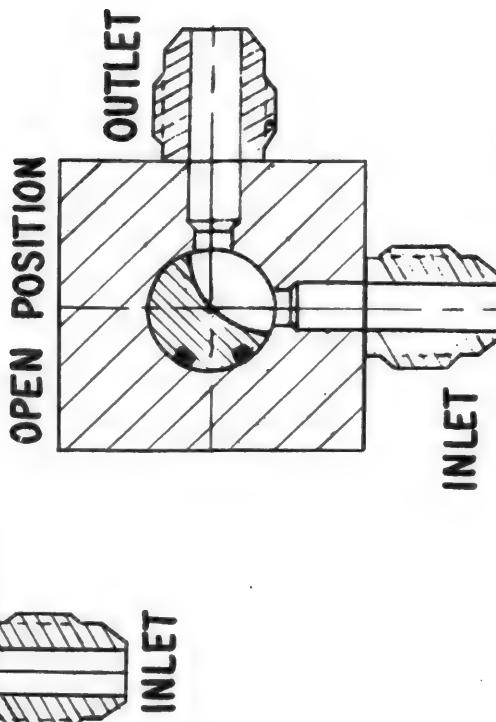
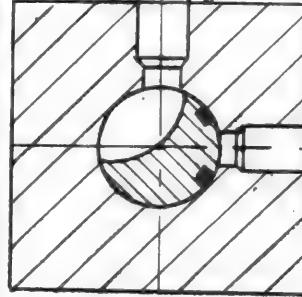
6. LIMIT LOAD TEST

TANK ISOLATION VALVE

OPERATING TOOL



CLOSED POSITION



OPEN POSITION

8250-472095-1

8250 COMPONENT PFRT TESTS

7. ACTUATION WITH FULL ΔP FORWARD (262 PSIG @ INLET, OUTLET OPEN TO ATMOS)
ACTUATION WITH FULL ΔP REVERSE (105 PSIG @ OUTLET, INLET OPEN TO ATMOS)
8. DYNAMIC TESTS

- a. SHOCK (6 MILLISECONDS DURATION AND A HALF SINE WAVE FORM, EACH SHOCK)
40 G, 3 SHOCKS IN BOTH DIRECTIONS OF EACH PLANE FOR A TOTAL OF 18 SHOCKS
- b. ACCELERATION (10 MINUTE DURATION EACH DIRECTION)
LONGITUDINAL AXES : 12G AFT, 4G FORWARD
LATERAL AXES : 3G EACH DIRECTION
- c. SINUSOIDAL VIBRATION (45 MINUTES SWEEP FOR EACH AXIS)
ALL 3 AXES : 5 TO 14 CPS @ $\frac{1}{2}$ " D.A.
14 TO 40 CPS @ 5.0 g
40 TO 400 CPS @ 7.5 g
400 TO 3000 CPS @ 20.0 g.
- d. RANDOM VIBRATION (5 MINUTES ALONG EACH AXES)
0.1 g²/CPS @ 15 TO 2000 CPS UTILIZING A 2 SIGMA CLIPPER

8101 COMPONENT DEVELOPMENT TESTS

PRESSURES	HIGH PRESSURE UNITS	LOW PRESSURE UNITS
OPERATING	3600 PSIG	255 PSIG
PROOF	5400 PSIG	383 PSIG
BURST	7200 PSIG	510 PSIG

TEST FLUIDS

- NITROGEN GAS MIL-P-27401 (USA) FOR GAS SYSTEM COMPONENTS
- METHYLENE CHLORIDE MIL-D-6998 FOR MON "
- METHANOL (METHYL ALCOHOL) O-17-232 FOR UDTHH "

TEMPERATURE TESTS

- HIGH TEMP : SOAK AT +160°F FOR 24 HRS - CONDUCT FUNCTIONAL TEST @ 100°F
- LOW TEMP : SOAK AT -65°F FOR 24 HRS - CONDUCT FUNCTIONAL TEST @ 0°F

ENDURANCE TEST

CONDUCT OPERATIONAL CYCLE LIFE (1000 TO 10,000 CYCLES)

8101 COMPONENT DEVELOPMENT TESTS

ALTITUDE TESTS

CONDUCT FUNCTIONAL TESTS AT A SIMULATED ALTITUDE
OF 262,000 FEET

RADIATION TESTS

EXPOSURE TO A TOTAL RADIATION DOSAGE OF 5×10^5 ROENTGENS

HUMIDITY, SAND & DUST, SALT SPRAY PER MIL-STD-810

ELECTRICAL TESTS ON START VALVE & 3-WAY SOLENOID

a. ELECTRIC STRENGTH

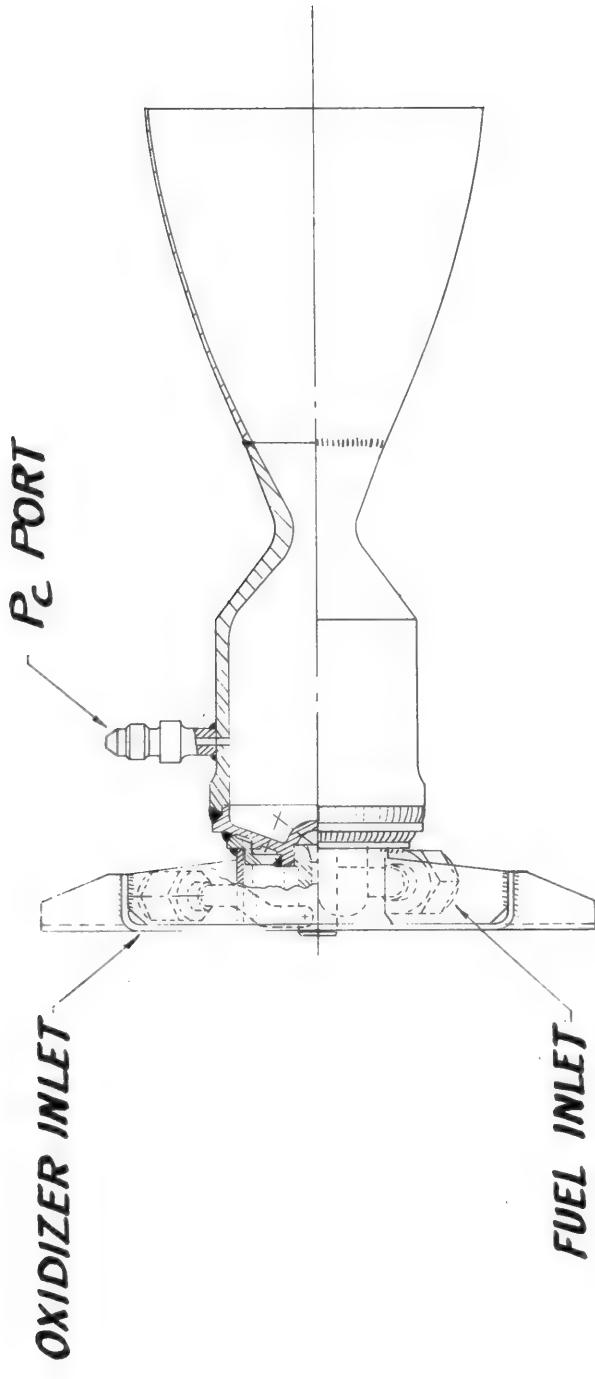
b. RESPONSE TESTS

8101 COMPONENT DEVELOPMENT TESTS

DYNAMIC TESTS

SHOCK —— 40G(3 SHOCKS, BOTH DIRECTIONS. EACH PLANE) 18 SHOCKS TOTAL
6 MILISECONDS DURATION & AN APPROX. HALF SINE WAVE FORM, EACH SHOCK
ACCELERATION—LONGITUDINAL AXIS, 12G AFT, 4G FORWARD - 10 MIN DURATION EACH
LATERAL AXIS, 3G EACH DIRECTION - 10 MIN DURATION EACH
SINUSOIDAL VIBRATION-(45 MINUTES ALONG EACH AXIS)
LONGITUDINAL AXIS 5 TO 15 CPS @ $\frac{1}{2}$ " D.A.
15 TO 40 CPS @ 3G
40 TO 400 CPS @ 7.5G
400 TO 3000 CPS @ 20G
LATERAL AXES 5 TO 15 CPS @ $\frac{1}{2}$ " D.A
15 TO 400 CPS @ 3 G
400 TO 3000 CPS @ 7.5G
RANDOM VIBRATION (5 MINUTES ALONG EACH AXES
.05g²/CPS @ 15 TO 2000 CPS UTILIZING A 2 SIGMA CLIPPER

UNIT I THRUST CHAMBER



UNIT I

I. NAME OF COMPONENT MODEL 82250 PART No. MODEL 8101 PART No.
THRUST CHAMBER ASSY. 82250-470001 8101-470075

II. TYPE OF COMPONENT AND GENERAL DESCRIPTION

RADIATION COOLED $F = 16 \text{ lb.}$ $P_c = 80 \text{ PSIA}$ $\theta = .5 - /150 \text{ SEC.}$
 $r = 1.10$ $A_e/A_t = 55.6$ $T_{spool min.} = 241 \text{ SEC.}$
PROPELLANT TEMPERATURE $0 - 100^\circ\text{F}$

III. COMPONENT HISTORY AND STATUS

A. EARLY 8101 TESTING

1. AMBIENT - DURABILITY
2. ELEVATED TEMPERATURE AND INVERSE TEMPERATURE

UNIT I

III B. REDESIGN

1. TOROIDAL MANIFOLD
2. MATERIAL CHANGES
3. FLAME DEFLECTORS
4. INTERNAL COATINGS
5. EXTERNAL COATINGS
- C. Q/A PROGRAM

IV MODEL 8101

A. DEVELOPMENT LEVEL TESTS (INFORMAL PFRT)

1. DURABILITY
2. INVERSE TEMPERATURE
 - 2. HIGH P_e
 - b. HIGH AND LOW τ $\left\{ \begin{array}{l} \tau = 1.35 - 1.15 \\ \tau = 0.90 - 1.10 \end{array} \right.$
 - c. 100°F OXIDIZER & 40°F FUEL
 - d. 40°F OXIDIZER & 100°F FUEL

UNIT I

IV. MODEL 8101 CONT. (DETAILED TESTS - INFORMAL PFR)

A. 3. ELEVATED ENVIRONMENT

- a. HIGH P_e
- b. 100°F PROPELLANTS
4. COLD TESTS (0°F PROPELLANTS & HARDWARE)
5. ULTRA-LOW COLD TESTS (0°F PROPS. - 20°F HARDWARE)
6. SIMULATED P.V. FAIL TO CLOSE
7. SIMULATED BLADDER RUPTURE
8. MALFUNCTION TESTS (SEE M.A. REPT.)
9. ALTITUDE TESTING TO DETERMINE $C_{f\infty}$

UNIT I

IV MODEL 8101 CONT.

B. COMPONENT LEVEL FORMAL PFRT

1. CALIBRATION TESTS

- a. 1-30 SEC. @ 100% RATED THRUST
- b. 2-30 SEC. @ 90% "
- c. 2-30 SEC. @ 110% "
- d. 1-30 SEC. @ 100% "
- e. 2-10 SEC. @ 100% "

2. SIMULATED BLADDER RUPTURE TESTS

- a. OXIDIZER
- b. FUEL

UNIT I

IV MODEL 8101 CONT.

C. SYSTEM LEVEL FORMAL PFRT SYSTEM No. 1 (S/N 204)

1. CHECKOUT
2. ENVIRONMENTAL TESTS
 - a. HIGH TEMPERATURE
 - b. HIGH HUMIDITY
 - c. LOW TEMPERATURE
3. SAFETY LIMITS
 - a. START SHUTDOWN
 - (1.) VARYING VOLTAGE
 - (2.) REFEREE PROPELLANTS
4. MALFUNCTION TESTS
 - a. START VALVE FAILURE
 - b. PROPELLANT VALVE FAILURE TO CLOSE
 - c. HIGH REGULATOR OUT PRESSURE (260 PSIA)
 - d. LOW REGULATOR OUT PRESSURE (150 PSIA)
 - e. SIMULATED FUEL EXHAUSTION
 - f. SIMULATED OXIDIZER EXHAUSTION

UNIT I

IV MODEL 8101 CONT.

D. SYSTEM LEVEL FORMAL PERT SYSTEM No. 2 (S/N 105)

	T/C S/N (IA)	T/C S/N (IB)
1. FIXED THRUST No. 1	8	13
2. FIXED THRUST No. 2	3	3
3. INVERSE TEMPERATURE No. 1	13	3
4. INVERSE TEMPERATURE No. 2	13	3
5. FIXED THRUST No. 3	13	3
6. FIXED THRUST No. 4	12	20

E. QUALIFICATION OF UNIT I

F. FLIGHT HISTORY

UNIT IV. MODEL 8250A. TYPE OF CHANGES (CHANGES FROM 8101)

1. CONTAMINATION CONTROL
2. FILTERS
3. PV GASKETS

B. PROBLEMS & CORRECTIONS

1. TRIM ORIFICE
2. FLOW RATES

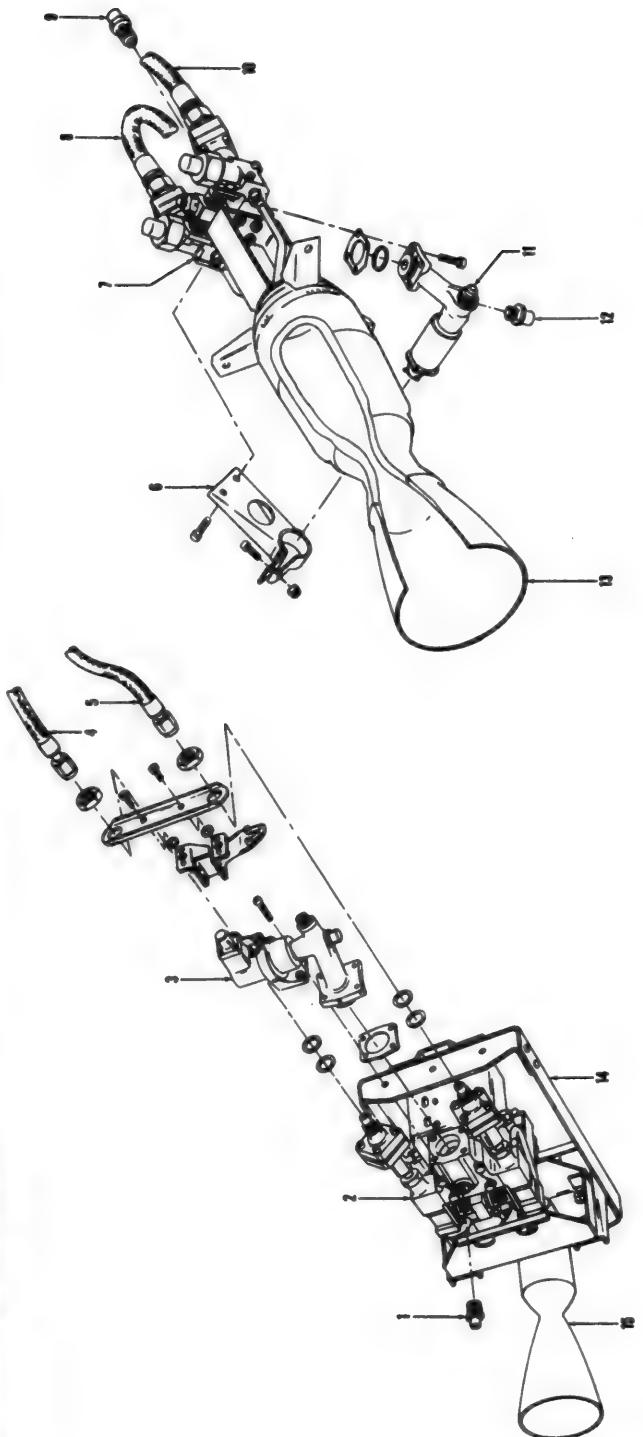
C. COMPONENT TESTING

1. Q/A PROGRAM
2. COAST TESTS
3. LOW TEMPERATURE LIMITS
4. TEMPERATURE RANGE

D. COMPONENT LEVEL PFRTE. SYSTEM LEVEL PFRT

Model 8250

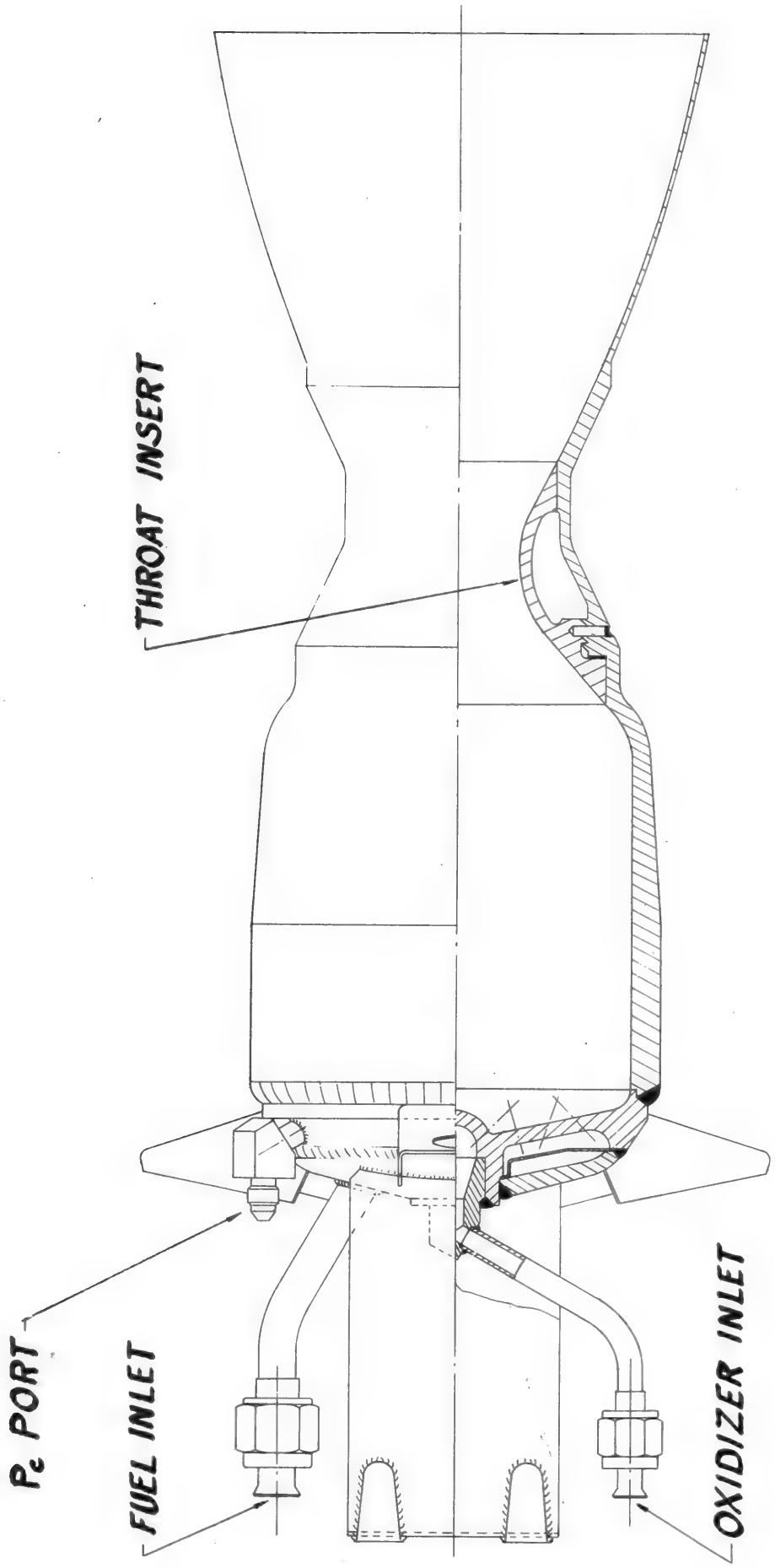
THRUST CHAMBER ASSEMBLIES (UNIT I & UNIT II)



1. Filter Assembly
2. Bi-propellant Valve
3. Solenoid Valve
4. Oxidizer Feed Line
5. Fuel Feed Line
6. Solenoid Support Bracket
7. Bi-propellant Valve
8. Fuel Feed Line
9. Filter Assembly
10. Oxidizer Feed Line
11. Solenoid Valve
12. Filter Assembly
13. Thrust Chamber, 200 lbs.
14. Support Bracket
15. Thrust Chamber, 16 lbs.



UNIT II THRUST CHAMBER



UNIT II

I. NAME OF COMPONENT MODEL 8250 PART No. MODEL 8101 PART No.
THRUST CHAMBER ASSEMBLY 8250-470010 8101-470010

II. TYPE OF COMPONENT AND GENERAL DESCRIPTION

HEAT SINK CHAMBER F-200 lb. $P_e = 96 \text{ PSIA}$ $\theta = .5 - 50 \text{ SEC'S.}$
 $r = 1.15$ $A_e/A_e^{room} = 15.6$ $T_{room} = 249 \text{ SEC'S.}$
PROPELLANT TEMPERATURES $0^\circ - 100^\circ F$

III. COMPONENT HISTORY AND STATUS

A. EARLY MODEL 8101 TESTING

1. AMBIENT DURABILITY
2. ELEVATED TEMPERATURE & INVERSE TEMPERATURE

UNIT II

III B. REDESIGN

1. CHAMBER WALL THICKNESS
2. NOZZLE WALL THICKNESS
3. TANTALUM NOZZLE GASKET
4. FLAME DEFLECTOR
5. BRACKET WELD

IV. MODEL 8101

A. DEVELOPMENT LEVEL TESTS (INFORMAL PFRT)

1. DURABILITY
2. INVERSE TEMPERATURES
 - a. HIGH P_c
 - b. HIGH & LOW τ
 - c. 100°F OX AND 40°F FUEL
 - d. 40°F OX AND 100°F FUEL

UNIT II

IV MODEL 8101 CONT. (DEV. LEVEL TESTS)

A. 3. ELEVATED ENVIRONMENT

- a. HIGH P_c
- b. 100°F PROPELLANTS
- c. COLD TESTS - (0°F PROPS. AND HARDWARE)
- d. ULTRA-LOW COLD TESTS (0°F PROPS. & -100°F HARDWARE)
- e. SIMULATED P.V. FAILURE TO CLOSE
- f. SIMULATED BLADDER FAILURE
- g. ALTITUDE TESTING TO DETERMINE $C_{f,\infty}$
- h. MALFUNCTION TESTS.

UNIT II

IV MODEL 8101 CONT.

B. COMPONENT LEVEL FORMAL PFRT

1. CALIBRATION TESTS

- a. 1-30 SEC. @ 100% RATED THRUST
- b. 2-30 SEC. @ 90% RATED THRUST
- c. 2-30 SEC. @ 110% RATED THRUST
- d. 2-10 SEC. @ 100% RATED THRUST

2. SIMULATED BLADDER RUPTURE TESTS

2. OXIDIZER

b. FUEL

C. SYSTEM LEVEL FORMAL PFRT SYSTEM NO.1 (S/N 204)

1. CHECKOUT TESTS

UNIT II

IV MODEL 8101 CONT. (SYSTEMS LEVEL FAIRING PFRT)

C. 2. ELEVATED ENVIRONMENT

a. HIGH TEMPERATURE

- (1.) B/0 - S/N-2 - EVALUATION PROGRAM
- (2.) P.V. POPPETS DEFORMED S/N-5

a. PENALTY TEST ON P.V @ PFRT

b. HIGH HUMIDITY

c. COLD TEST

- (1.) P.V. BELOW S/N-5 T.C.A. (J. PIRRONI) TRT (855 SEC'S.)
- (2.) S/N-12 DID NOT FUNCTION. THROAT PLUG FELL OUT - CO_2 REACTED WITH UDTH & PLUGGED FUEL SIDE

3. SAFETY LIMITS

a. START SHUTDOWN

- (1.) VARYING VOLTAGE
- (2.) REFEREE PROPELLANTS

UNIT II

IV MODEL 8101 CONT. (SYSTEMS LEVEL FORMAL PFRT)

C. 2. C. 4. MALFUNCTION TESTS

2. START VALVE FAILURE
 - b. PROP VALVE FAIL TO CLOSE
 - c. HIGH REGULATOR OUT PRESSURE (260 PSIA)
 - d. LOW REGULATOR OUT PRESSURE (150 PSIA)
 - e. SIMULATED FUEL EXHAUSTION
 - f. SIMULATED OXIDIZER EXHAUSTION
- D. SYSTEM LEVEL FORMAL PFRT SYSTEM No. 2 (S/N 105)
 1. FIXED THRUST No. 1
 2. FIXED THRUST No. 2
 3. INVERSE TEMPERATURE No. 1
 4. INVERSE TEMPERATURE No. 2

UNIT II

IV. MODEL 8101 CONT. (SYSTEMS LEVEL FORMAL PFRT SYSTEM NO.2)

- D. 5. FIXED THRUST No. 3
- 6. FIXED THRUST No. 4
 - a. T.C. S/N-8 TRT - 556 SEC'S.
 - b. T.C. S/N-10 TRT - 510 SEC'S.

E. QUALIFICATION OF UNIT II

F. FLIGHT HISTORY.

V. MODEL 8250

- A. TYPE OF CHANGES (CHANGES FROM 8101)
 - 1. CONTAMINATION CONTROL
 - 2. FILTERS
 - 3. P.V. GASKET

UNIT II

V MODEL 82250 cont.

B. PROBLEMS AND CORRECTIONS

1. TRIM ORIFICE
2. FLOW RATES
3. WRAP AROUND PADS

C. COMPONENT TESTING

1. HIGH FEED PRESSURE DECAY
2. COAST TESTS - PREDICTED FROM 82250 ANALYSIS/S
3. LOW TEMPERATURE LIMITS FROM 8/101 UNIT I TESTS & 82250 ANALYS.
4. BURNOUT INVESTIGATION
- D. COMPONENT LEVEL PFRT
- E. SYSTEM LEVEL PFRT

MODEL 8250 S.P.S. TANKS

NAME - TANKS-FUEL AND OXIDIZER

THE MODEL 8250 PROPELLANT TANKS ARE POSITIVE EXPULSION DEVICES UTILIZING A 347 SS WELDED BELLOWS INSIDE OF AN A286 CYLINDRICAL SHELL. BOTH OX & FUEL TANKS ARE SIMILAR EXCEPT FOR LENGTH & NUMBER OF CONVOLUTIONS.

FUNCTION -

THE FUNCTION OF THE BELLOWS TANKS IS TO STORE THE PROPELLANTS & ON DEMAND, TO PROVIDE THE SPS THRUST UNITS WITH A CONTINUOUS FLOW OF LIQUID PROPELLANTS.

COMPONENT HISTORY -

THE BELLOWS CONCEPT AS A POSITIVE EXPULSION DEVICE FOLLOWED THE 8101 BLADDER TANKS. THE NEED FOR A MORE RELIABLE DEVICE INDICATED THE USE OF A BELLOWS TANK. A DEVELOPMENT PROGRAM WAS INSTITUTED & PERFORMED.

STATUS -

THE TANKS ARE BEING PROVIDED IN THE FOLLOWING CONFIGURATIONS -
8250-471301-1 FUEL TANK
8250-471302-1 OXIDIZER TANK

TYPE OF TESTING -

THE MODEL 8250 TESTING WAS CONDUCTED WITH BELLows OF $7\frac{1}{8}$ INCH DIAMETER & 10 INCH DIAMETER. THESE TESTS DEMONSTRATED THE FOLLOWING -

- A - FLOW & TRAVEL CHARACTERISTICS
- B - VOLUME, SPRING RATE & HYSTERESIS
- C - DYNAMICS CHARACTERISTICS
- D - COMPATIBILITY WITH PROPELLANTS
- E - CONTAMINATION CONTROL CAPABILITY

THESE TESTS WERE CONDUCTED WITH VARIOUS LENGTHS OF BELLows. SOME OF THE TESTED BELLows HAD 10, 20, 95, 135 & 149 CONVOLUTIONS.

PROBLEMS & CORRECTIVE ACTIONS (C.A.)

1 SHELL PROBLEM - WELD CRACKING ENCOUNTERED DURING FABRICATION.

- C.A. - A. RIGID REQUIREMENTS IMPOSED ON A286 MAT'L CHEMISTRY
- B. PLATE OR FORGED BILLET REPLACED BY CLOSED DIE FORGING
- C. FIXTURING & PROCESS IMPROVEMENTS -
(CHILL BARS, BACK UP RINGS, TEMPERATURE CONTROL)

2 BELLOWS PROBLEMS -

A-BELLOW FAILURE IN VIBRATION DURING ACCORDIAN MODE-

- C.A. - ADDITION OF BELLOWS BAFFLES TO ATTENUATE ACCORDIAN MODE
2 BAFFLES IN OX BELLOWS & 3 BAFFLES IN FUEL BELLOWS
- B - BELLOW FAILURE IN RANDOM VIBRATION

C.A. - RELIEF GRANTED BY LMSC

C - BELLOW COCKING DURING FILL CYCLE

- C.A. - REDUCE DEVIATIONS IN BELLOWS TRAVEL BY NORMALIZING BELLOWS
- CONTROL SHELL SIZE & OVALITY BY TIGHTER FABRICATION CONTROL
- TEFLON COATING ON OUTER EDGE OF MOVEABLE HEAD (A TEFLON COATED TEST BELLOW WAS CYCLED OVER 80 TIMES IN ATTITUDES VARYING FROM VERTICAL TO HORIZONTAL. THE INCREMENTS OF DEFLECTION WERE FROM 1° TO 90°)

QUALIFICATION -

QUALIFICATION WAS PERFORMED DURING DEVELOPMENT TESTING AND DURING THE SYSTEM PFRT TESTING

- A - A TANK WITH A TEFLON COATED HEAD WAS SUBJECTED TO RANDOM LATERAL VIBRATION. THE COATING WAS SLIGHTLY ABRADED BUT ENOUGH TEFLON REMAINED TO INSURE SMOOTH TRAVEL
- B - 3 PROTOTYPE & 6 TEST TANKS WERE TESTED TO HIGH LEVEL DYNAMICS REQUIREMENT. 3 MORE PROTOTYPE TANKS WERE TESTED SATISFACTORILY TO THE REDUCED DYNAMICS LEVEL. IN ADDITION, A SYSTEM WITH TANKS WAS SUBJECTED TO FORMAL PFRT SYSTEM DYNAMIC LEVELS SATISFACTORILY. THESE PFRT TANKS WERE THEN EXPULSION CYCLED TO 201 (OX) & 207 (FUEL). THE SHELLS WERE THEN PRESSURE CYCLED, PROOF TESTED & BURST. (OX 596*, FUEL 606*) PROBLEMS TO QUALIFIED HARDWARE & CORRECTIVE ACTION (C.A.)
- A- CREVICE CORROSION CAUSED BY CHEMICAL ATTACK ON EDGE OF WELD C.A. (PROPOSED) 1- INHIBIT THE NITRIC ACID PASSIVATING SOLUTIONS.
- 2- REVISE PROCESSING TO ELIMINATE ALL H.F. SOLUTIONS.
- 3- RIGID HEAT TREAT CONTROL TO REDUCE DISCOLORATION & SCALING.
- 4- MECHANICAL CLEANING OF HEAT TREATED PARTS & WITH INHIBITED PASSIVATING SOLUTIONS ONLY.

GAS BOTTLE - (8101-471001-3 & 8250-471030-1)

THE GAS BOTTLE IS A TITANIUM SPHERE USED TO STORE NITROGEN GAS AT HIGH PRESSURE FOR USE AS REQUIRED IN THE SYSTEM TO EFFECT A TRANSFER OF PROPELLANTS TO THE THRUST UNITS.

THE GAS BOTTLE WAS QUALIFIED ON THE 8101 PROGRAM. SEVERAL BOTTLES WERE PRESSURE CYCLED, PROOF TESTED TO 6000 PSIG & BURST TESTED. (BURST PRESSURES WERE APPROXIMATELY 9200 TO 9555 PSIG WHICH IS WELL IN EXCESS OF DESIGN BURST-8000 PSIG)

CHANGES TO THE GAS BOTTLE SINCE QUALIFICATION -
ADDED A CONTAMINATION CONTROL REQUIREMENT &
CHANGED THE PART NUMBER TO REFLECT MODEL 8250.

MODEL 8250 FLIGHT HISTORY - NONE

PROPELLANT TANK DYNAMIC REQUIREMENTS

SHOCK

LONGITUDINAL AXIS
LATERAL AXES

35 g
15 g

ACCELERATION

LONGITUDINAL AXIS
LATERAL AXES

12 g FORWARD 1g AFT
 ± 3 g

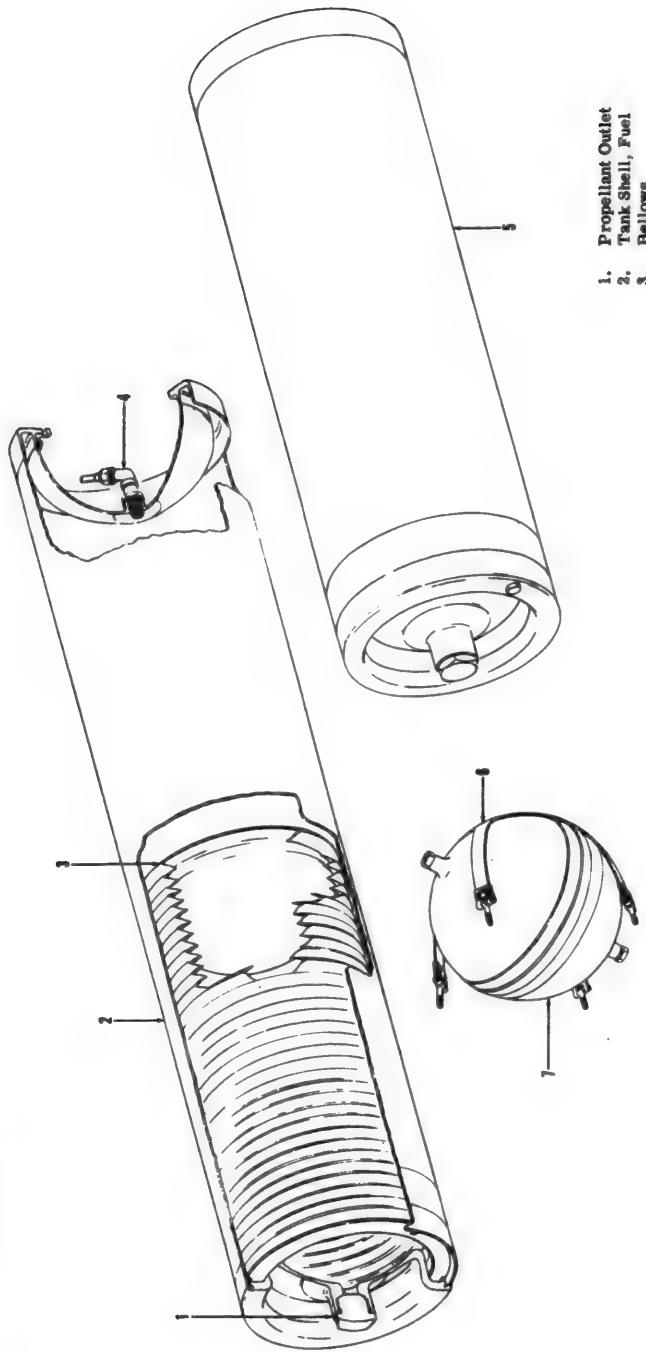
SINUSOIDAL VIBRATION

LONGITUDINAL AND
LATERAL AXES

0.5 TO 5 CPS AT $\frac{1}{4}$ INCH SINGLE AMPLITUDE
5 TO 11 CPS AT $\frac{1}{8}$ INCH SINGLE AMPLITUDE
11 TO 90 CPS AT 1.5 g
90 TO 600 CPS AT 2.0 g

Model 8250

TANK ASSEMBLIES



1. Propellant Outlet
2. Tank Shell, Fuel
3. Bellows
4. Gas Inlet
5. Oxidizer Tank
6. Strap Assembly
7. Nitrogen Tank

E3644
© 1987 E3644

MODEL 8101 SYSTEM

- 1. COMPONENTS MOUNTED IN VARIOUS AREAS OF VEHICLE*
- 2 COMPLEX CONFIGURATION*
- 3 R & D TESTING*
- 4. PFRT TESTING*

MODEL 8250 SYSTEM

- 1. MODULAR CONCEPT*
- 2 SIMPLIFIED CONFIGURATION*
- 3. CONTAMINATION CONTROL*

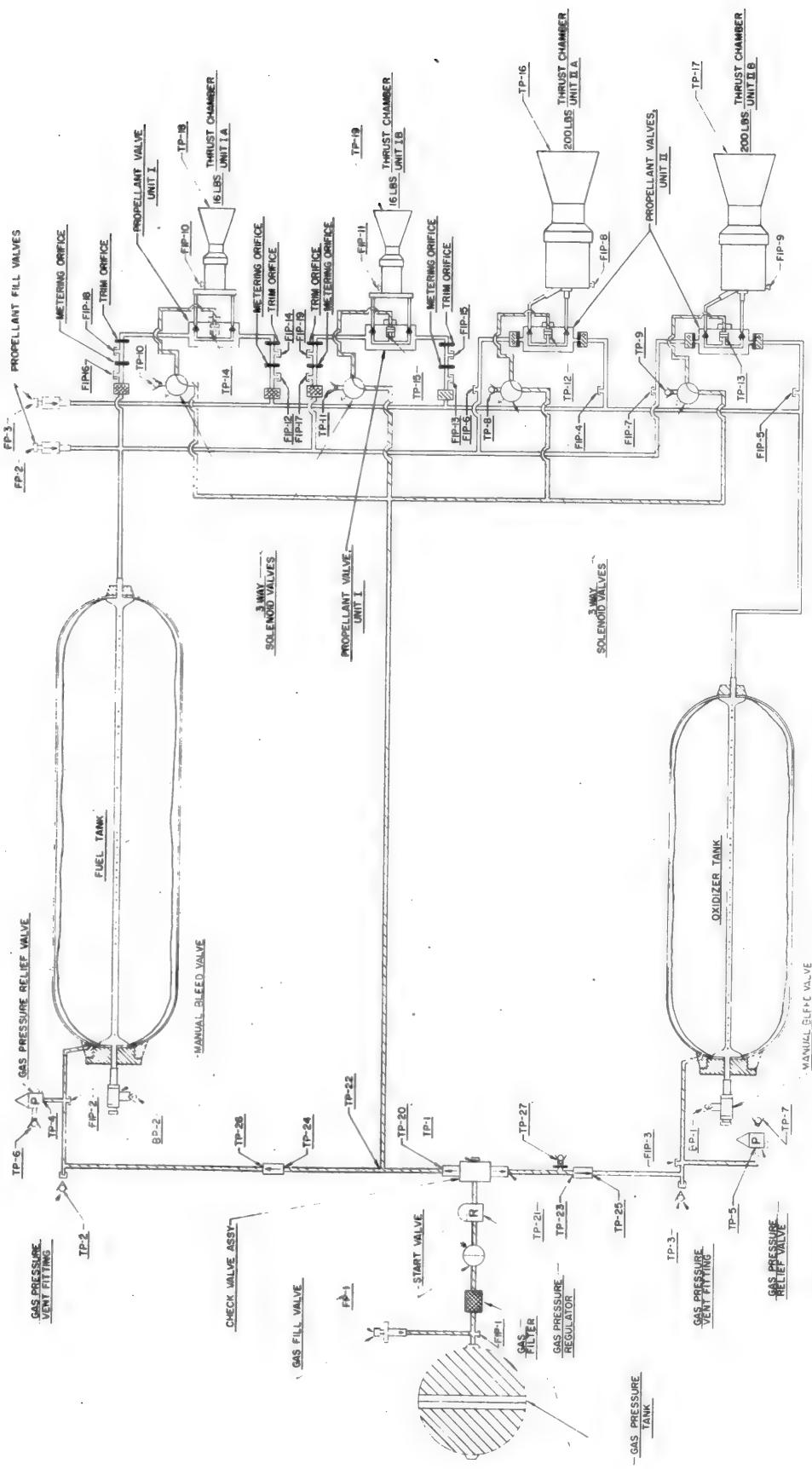
MODEL 8101 SYSTEM

- 1. COMPONENTS MOUNTED IN VARIOUS AREAS OF VEHICLE*
- 2 COMPLEX CONFIGURATION*
- 3 R & D TESTING*
- 4. PFRT TESTING*

MODEL 8250 SYSTEM

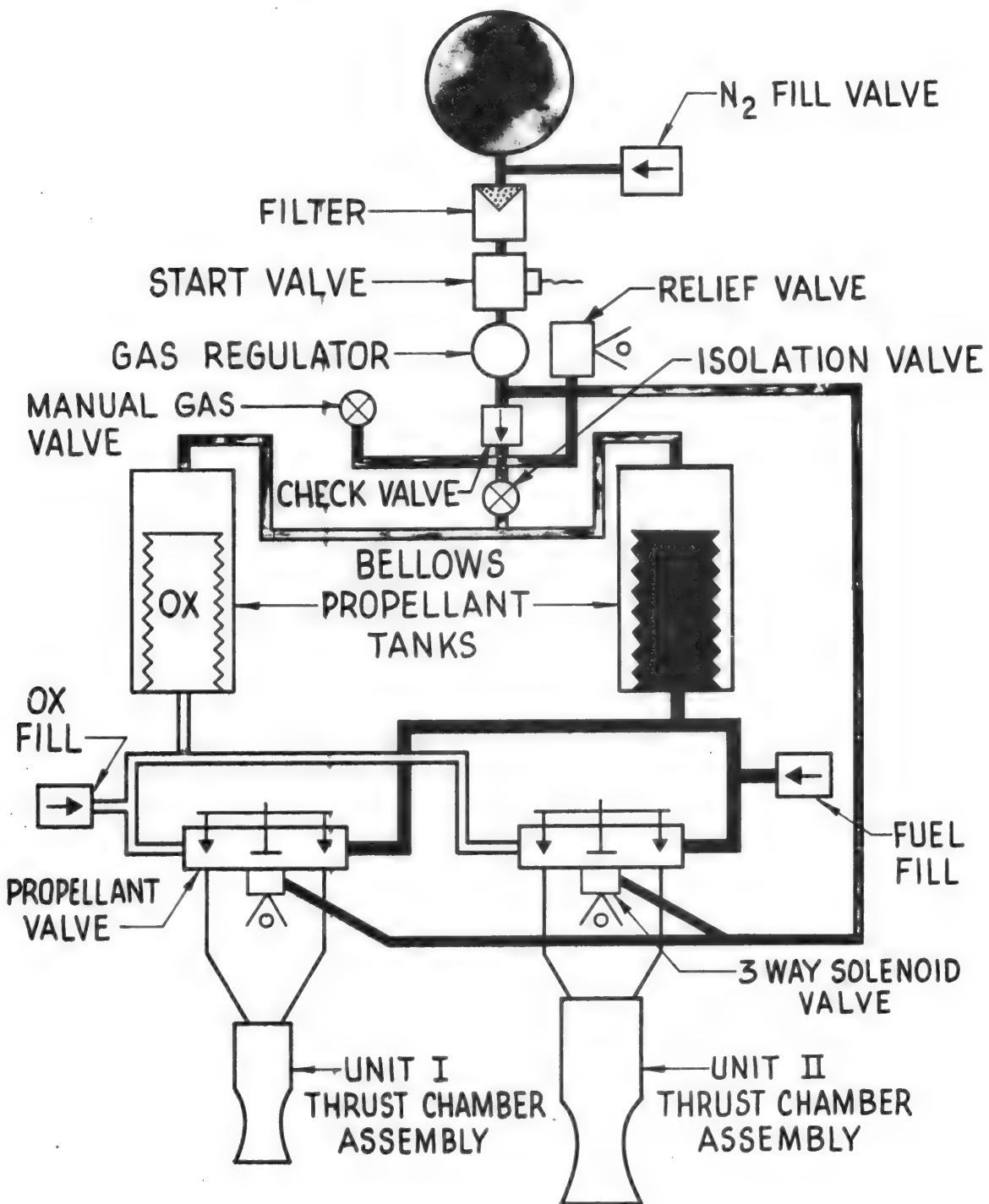
- 1. MODULAR CONCEPT*
- 2 SIMPLIFIED CONFIGURATION*
- 3. CONTAMINATION CONTROL*

MODEL 8101 SYSTEM



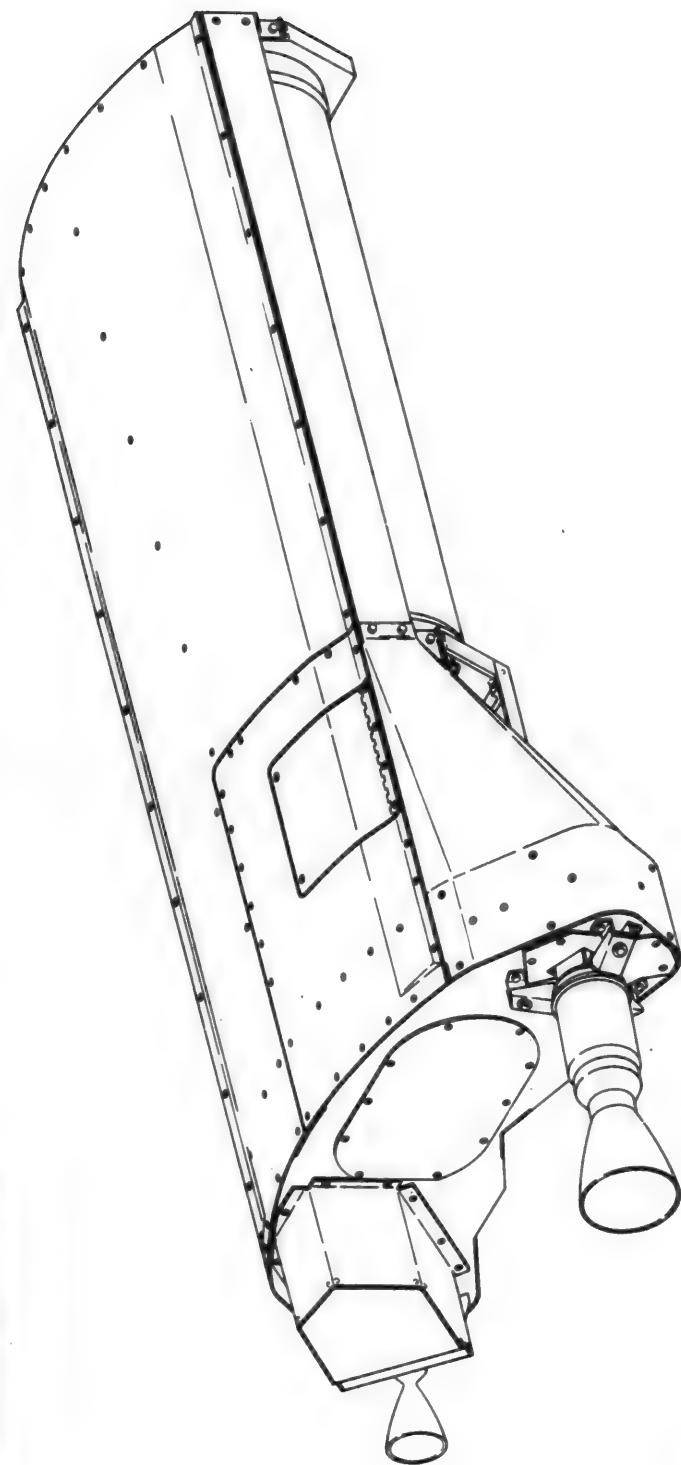
140

MODEL 8250 SYSTEM WITH BELLOWS TANKS



Model 8250

MODULE - SECONDARY PROPULSION SYSTEM



Model 8250

MODULE COMPONENTS

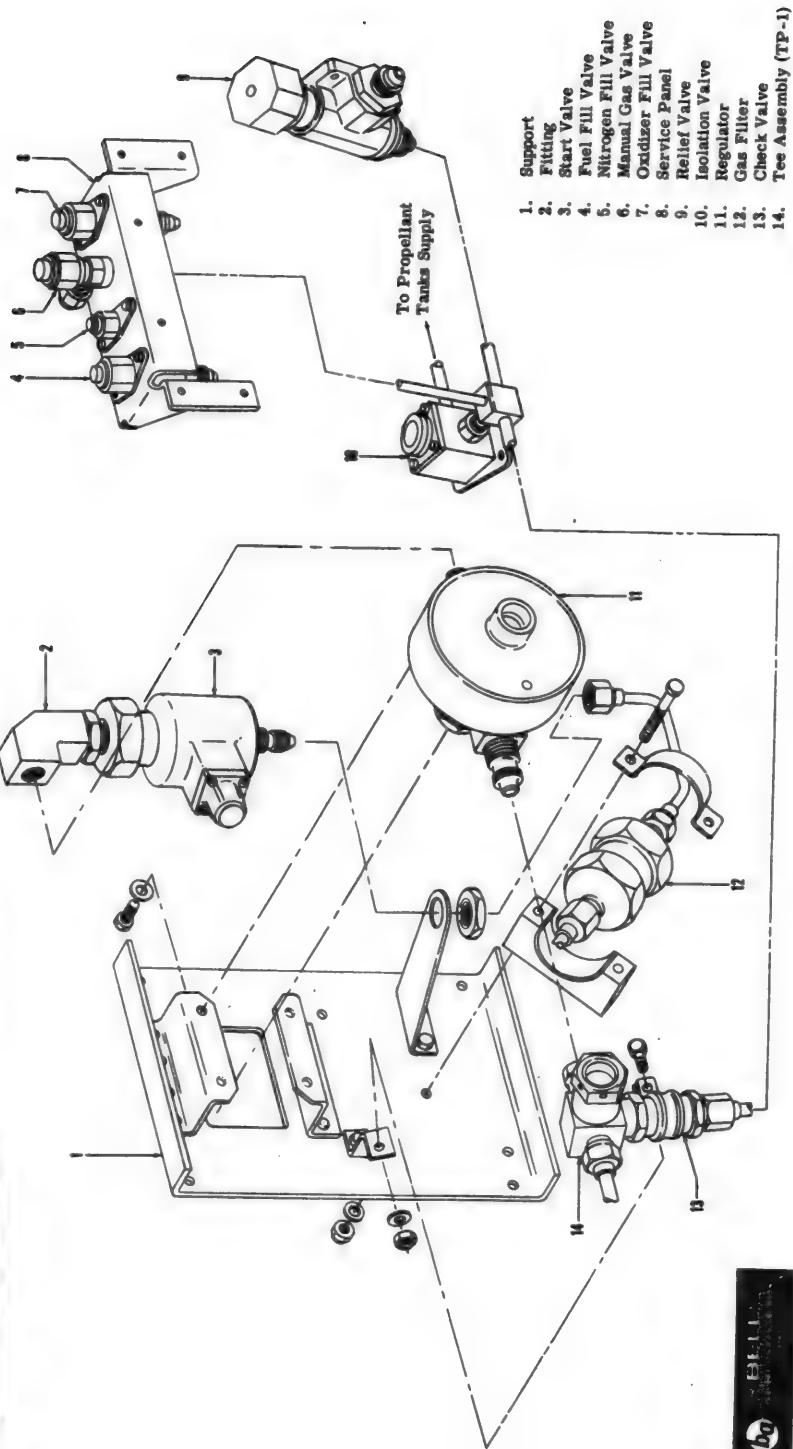


1. Nitrogen Tank
2. Pressurization Assembly
3. Cover, Tanks
4. Fuel Tank
5. Oxidizer Tank
6. Frame Assembly
7. Service Panel
8. Relief Valve
9. Isolation Valve
10. Cover, Unit II Support
11. Unit II Closures
12. Unit II Thrust Chamber Assembly
13. Cover, Unit I Support
14. Unit I Thrust Chamber Assembly
15. Cover, Unit I Support



Model 8250

PRESSURIZATION COMPONENTS



R AND D DYNAMIC TEST ON SYSTEM T-1

DESCRIPTION OF SYSTEM DYNAMIC LEVELS PROBLEMS

1. CRACK NOTED IN 8250-460017 BULKHEAD: REDESIGN OF CORNER AND ADD GUSSET. 8250-46016 BULKHEAD WAS CHANGED IN LIKE MANNER
2. CRACK NOTED AT THE UNIT II THRUST CHAMBER PROPELLANT VALVE MOUNTING PADS: REDESIGN OF DOUBLER PADS
3. RUBBING NOTED BETWEEN UNIT I X FEED FLEX LINE AND UNIT I COVER: LINE POSITION WAS ADJUSTED
4. LOSS OF APPROX 45 POUNDS OF SIMULATED PROPELLANT DUE TO TEST LINES AND VALVES: ANALYSIS INDICATED NO PROBLEM WOULD BE ENCOUNTERED AT MAX WEIGHT DURING PERT

-fsc

R & D FIRE TESTING ON SYSTEM S/N T-2

SEVEN TESTS CONDUCTED ON SYSTEM T-2 INCLUDED, AMBIENT,
HIGH TEMPERATURE AND LOW TEMPERATURE TESTS

PROBLEMS

1. GAS FILL VALVE INSTALLED BACKWARDS; NOTCH ADDED TO FLANGE ON VALVE AND PIN ADDED TO SERVICE PANEL
2. PORT ON UNIT II SOLENOID VALVE COULD NOT BE REACHED; A HOLE WAS ADDED TO THE STRUCTURE
3. FUEL TANK S/N 4 BELLOW HEAD COCKED; TANK HEAD FREED AND TANK REINSTALLED
4. GAS REGULATOR OUT OF SPEC. AFTER 3RD TEST; REDESIGN AND REGULATOR TEST PROGRAM
5. GAS FILL VALVE LEAKING; SHRED OF TEFLON ON SEAT
6. FUEL TANK S/N 4 DAMAGED DUE TO TESTING ERROR; PROCEDURE CHANGES
7. UNIT II TCA FAILURE ON HOT TEST; "BURN OUT" PROGRAM
8. PROPELLANT LOADING DISCREPANCY; CHANGES TO PROCEDURES AND CHECKS ON CALIBRATION METHODS

MODEL 8250 SYSTEM PFRT

SINUSOIDAL VIBRATION AND ACCELERATION TESTS

SINUSOIDAL VIBRATION *

LONGITUDINAL AXIS

5 TO 11 CPS AT 0.125 INCH SINGLE AMPLITUDE
// TO 90 CPS AT 1.5g
90 TO 1000 CPS AT 2.0g

LATERAL AXES

5 TO 11 CPS AT 0.125 INCH SINGLE AMPLITUDE
// TO 1000 CPS AT 1.5g

THE VIBRATION WAS APPLIED AT A CONSTANT OCTAVE SWEEP FROM THE LOWEST TO THE HIGHEST FREQUENCY IN 24 MIN.

ACCELERATION *

LONGITUDINAL AXIS

1/2 g FORWARD
1 g AFT
 $\pm 3 \frac{1}{2}$ g

LATERAL AXES

THE ACCELERATION WAS APPLIED FOR 10 MINUTES EACH DIRECTION PARALLEL TO THE INDICATED SATELLITE AXIS

* SYSTEM FULLY LOADED WITH TEST FLUIDS AND PRESSURIZED TO OPERATING PRESSURES EXCEPT THE GAS PRESS. TANK WAS PRESSURIZED TO 2230 PSIG WITH ARGON

MODEL 8250 PFRT

QUALIFICATION

PRE-PFRT TESTING
SYSTEM ACCEPTANCE TEST WITH TEST TANKS
PROPELLANT TANK SET $\frac{5}{8}$ " - CYCLED PRIOR TO INSTALLATION

DYNAMIC TESTS

STATIC LEAKAGE AND FUNCTIONAL TEST
HELI-COIL INSTALLATION IMPROPER

ACCELERATION TESTING

POST ACCEL. PRESS. CHECKS - LEAK AT GAS END OF OX TANK

SINUSOIDAL VIBRATION

PRE-TEST - POSITION STRIPE ON RELIEF VALVE
ADJUSTMENT CAP MISSING

X AXIS VIBRATION

GAS PRESS. TANK MOUNTING SCREWS TORQUED TO 25 IN. LB

MODEL 8250 PFRT

Z AXIS VIBRATION
RIPPLES IN OXIDIZER TANK
Y AXIS VIBRATION
POST DYNAMIC TEST PRESSURE CHECKS
PREPARE FOR SHIPMENT TO BTC FUEL VALVE LEAKING

FIRE TEST

STATIC LEAKAGE AND FUNCTIONAL CHECK
PFRT FIRE TEST INCLUDED FIXED THRUST TESTS, HUMIDITY,
AND HIGH & LOW TEMPERATURE TESTS
PROBLEMS

FIXED THRUST TESTS
UNIT I PROPELLANT VALVE FAILURE DUE TO SALTS ON
OXIDIZER SIDE; GOLD GASKETS INSTALLED
HIGH TEMPERATURE TEST
UNIT II THRUST CHAMBER BURN-OUT

MODEL 8250 PFRT

HUMIDITY TESTS

CORROSION IN STAGNANT AREAS & WHERE ANODIZE
COATING WAS BROKEN

RUST ON SOLENOID VALVE

HEAT CONDUCTION STRAP CORROSION

COLD TEST

LEAKS AT TEFILON O'RING SEALS ; DESIGN CHANGE

LEAKS AT TUBING CONNECTION ; TORQUE CHECKS INITIATED

FINAL STATIC LEAKAGE AND FUNCTIONAL CHECK

MODEL 8250 LAUNCH HOLD PROGRAM

TEST CONDUCTED TO DEMONSTRATE WET AND DRY HOLD CAPABILITY
TEST CONDUCTED ON DELIVERABLE SYSTEM S/N 4

TEST

NORMAL ACCEPTANCE - TEST
20 DAY DRY STORAGE WITH TEMPERATURE CYCLE
INSTRUMENTATION INSTALLATION
20 DAY WET STORAGE WITH PROPELLANTS LOADED
RE-ACCEPTANCE TEST WITH 5 DAY COAST
DATA

RELIABILITY PROGRAM - MODELS 8247 & 8250

PROGRAM INITIATED — OCTOBER 15, 1963

COMPLETION DATE — APRIL 30, 1966

PROGRAM TASKS

PROGRAM PLAN

INDOCTRINATION

MOTIVATORS

FILMS

DOCUMENTATION REVIEW

PROCESS & MATERIAL SPEC

E. O. CHANGES

DESIGN SUPPORT

DESIGN REVIEW

FAILURE MODES & EFFECTS ANALYSIS

STATUS MEETINGS

ANALYSIS SERVICE

FAILURE ANALYSIS

BAC PROCEDURE

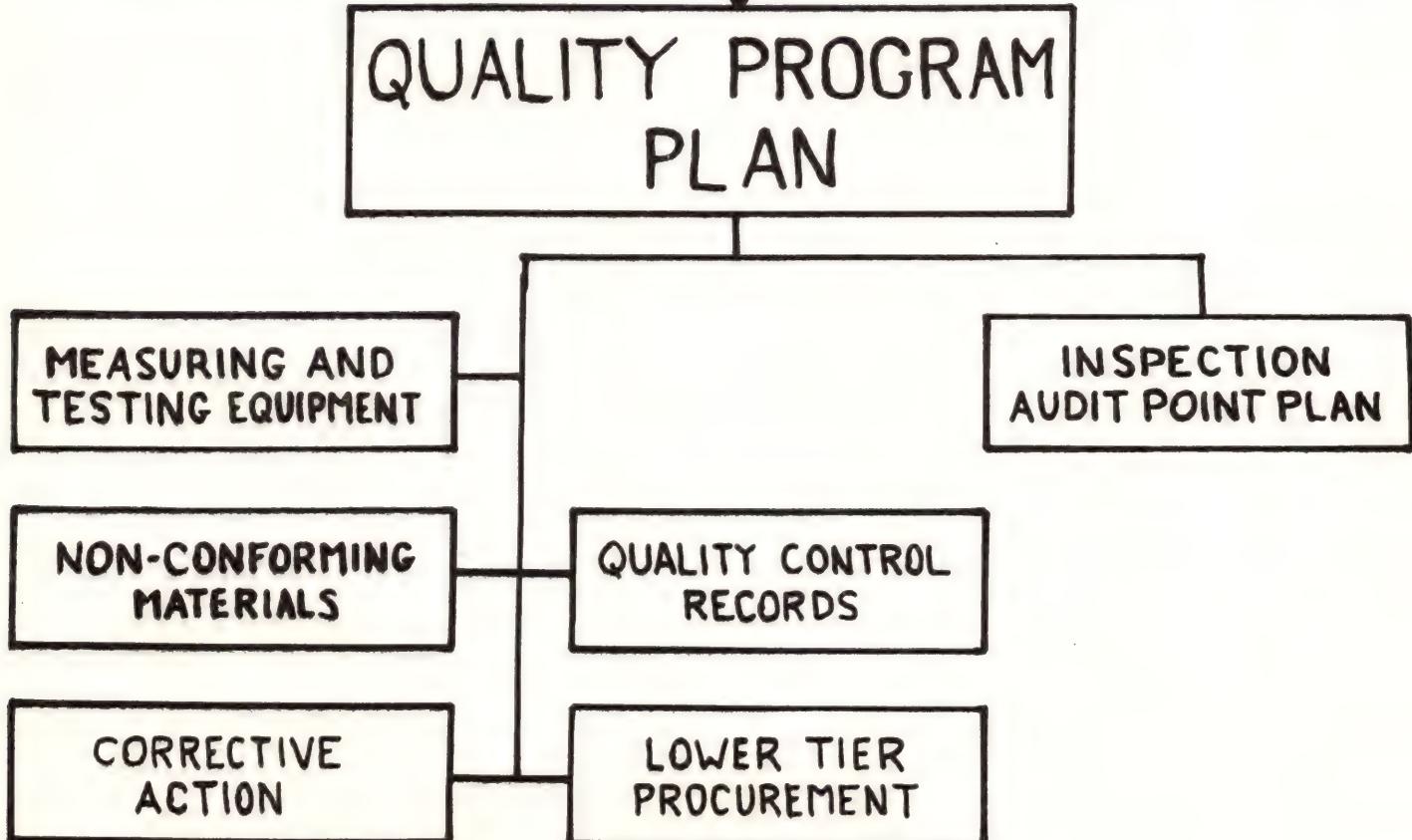
RELIABILITY PROGRAM - MODELS 8247 & 8250

SUPPLIER REVIEW	DATA REVIEW
FUNCTIONAL TEST	COLLECT & RECORD DATA
SPECIFICATIONS & DRAWINGS	TEST DATA ANALYSIS
SUB-CONTRACTOR PERFORMANCE	
MANUFACTURING ASSURANCE	PROGRAM REPORTS
AREA REVIEW	RELIABILITY MONTHLY
PROCESSES	QUARTERLY ESTIMATE



QUALITY PROGRAM REQUIREMENTS MIL-Q-9858

LMSC PRODUCT ASSURANCE
SUB-CONTRACT REQUIREMENTS
LMSC-A372550-MODEL 8250
LMSC-A067479-MODEL 8247





QUALITY DEPARTMENT

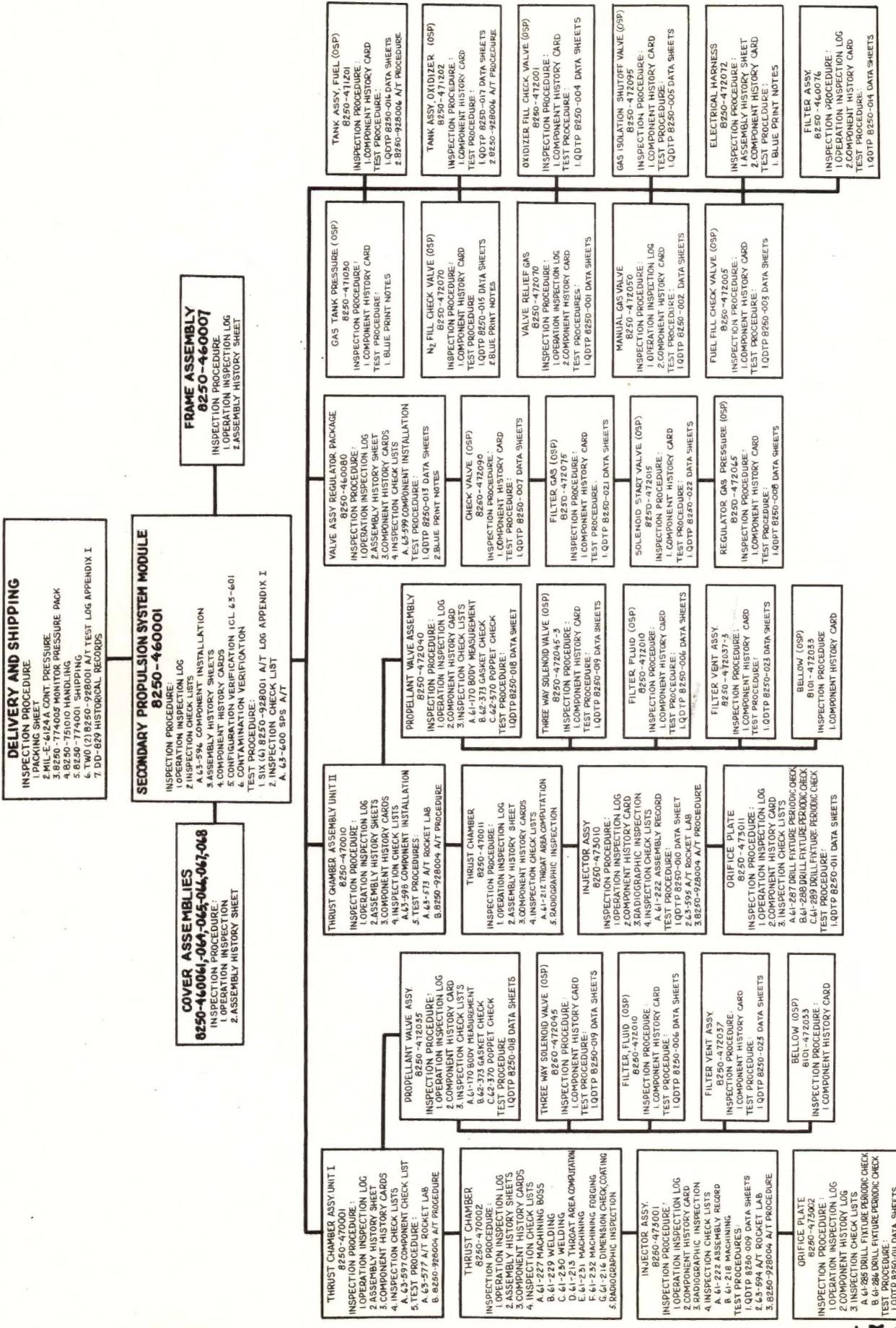
BAC MODEL 8247 - AF INSPECTION AUDIT POINT PLAN

DATE 5-10-64
APPROVAL 9. T. Bait

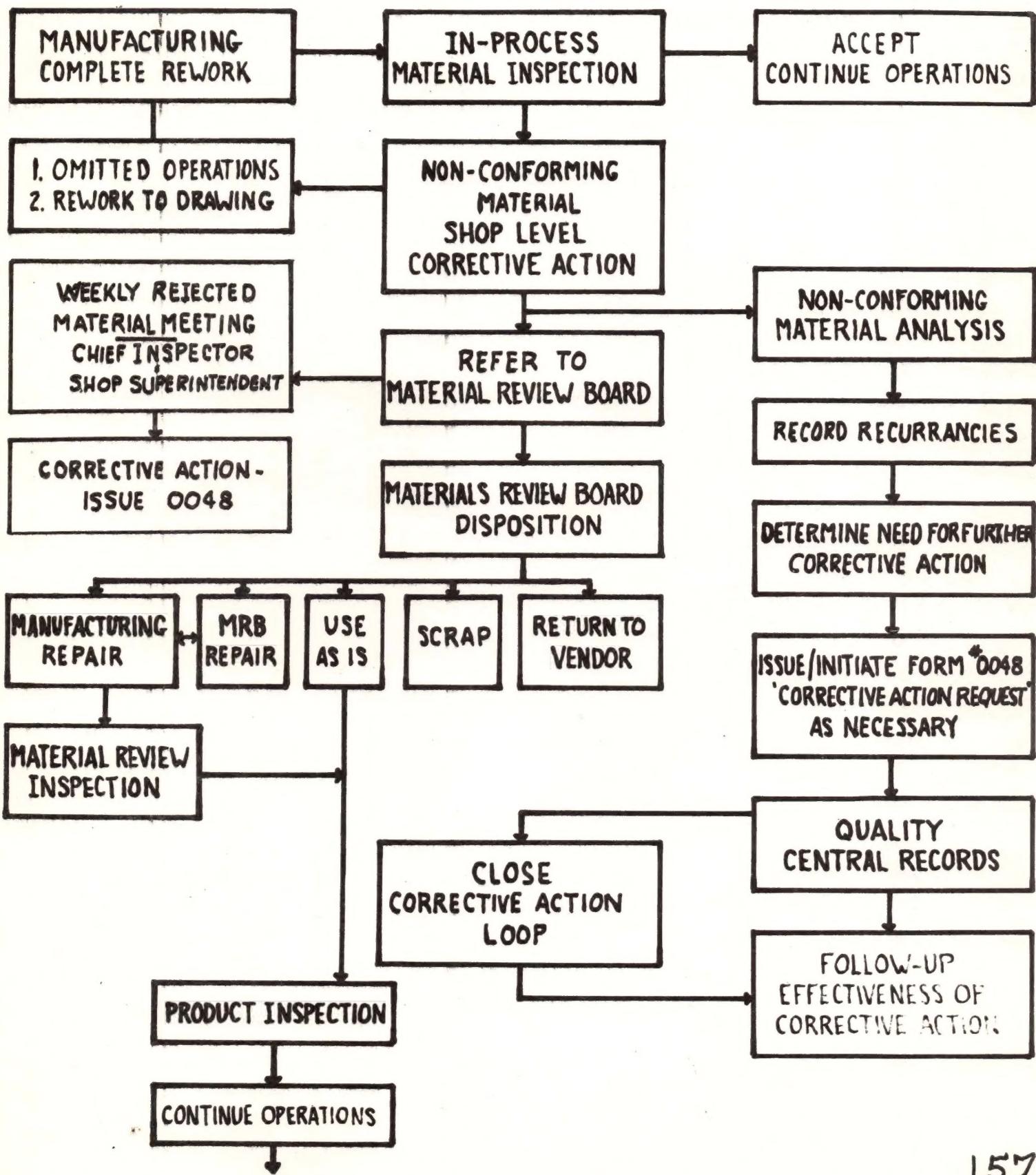


INSPECTION AUDIT POINT PLAN FOR MODEL 8250 SECONDARY PROPULSION SYSTEM MODULE

DATE **12-5-64**
APPROVAL **9/18/64**



HANDLING OF NON-CONFORMING MATERIAL



QUALITY FLOW CHART

VENDOR/SUB-CONTRACTOR CONTROLS

